

The ATF Damping Ring Beam Position Monitor System

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Fermilab

for the ATF Damping Ring BPM Team



- Motivation & “History”
- The ATF Damping Ring
- **BPM Upgrade Hardware**
- Results of Beam Studies
- Summary

- ILC damping ring R&D at KEK's Accelerator Test Facility (ATF):
 - Investigation of the beam damping process (damping wiggler, minimization of the damping time, etc.)
 - Goal: generation and extraction of a reproducible low **emittance beam** ($\epsilon_{\text{vert}} < 2 \text{ pm-rad}$) at the nominal ILC bunch charge
- A major tool for low emittance corrections:
a high resolution BPM system
 - Optimization of the closed-orbit, beam-based alignment (BBA) studies to investigate BPM offsets and calibration.
 - Correction of non-linear field effects, i.e. coupling, chromaticity,...
 - (Fast) global orbit feedback(?)
 - **Necessary: a state-of-the-art BPM system, utilizing**
 - a broadband turn-by-turn mode ($< 10 \text{ }\mu\text{m}$ resolution)
 - a narrowband mode with high resolution ($\sim 100 \text{ nm}$ range)
- ATF BPM read-out system upgrade
 - Button BPMs and signal cabling remains unchanged
 - New flexible BPM read-out system, tailored to ATF needs and requirements

- **ATF Damping Ring Beam Position Monitor System**
 - Button style BPM pickup stations
 - Original read-out electronics:
Analog signal processing, no TBT, intensity dependence
- **2006: M. Ross & SLAC team**
 - Analog downconverter & digital receiver (*Echotek*) read-out system, prototype achieves 1-2 μm resolution
- **2007/8: KEK/SLAC/Fermilab collaboration**
 - Beam tests of 20 BPMs in both arcs, equipped with new read-out system
 - EPICS & LabVIEW software
 - Achieved $<10 \mu\text{m}$ resolution in TBT, $\sim 200 \text{ nm}$ in narrowband mode
 - First test of an integrated automatic calibration system
- **2009: KEK/Fermilab**
 - Improvements on the analog downconverter
 - CAN-bus controls, IF filter, remote diagnostics, etc.
 - Switch to in-house VME digitizer (as of LHC delays: no Tevatron BPM *Echotek*'s)
 - 8-ch. ,125 MSPS ADC (serial outputs), Cyclone III FPGA, PLL-locked CLK distribution
 - New RF, DC & CAN-bus distribution. Grounding of tunnel hardware.

Machine and Beam Parameters

beam energy $E = 1.28 \text{ GeV}$

beam intensity, single bunch $\approx \sim 1.6 \text{ nC} \equiv 10^{10} e^- (\equiv I_{\text{bunch}} \approx 3.46 \text{ mA})$

beam intensity, multibunch (20) $\approx \sim 22.4 \text{ nC} \equiv 20 \times 0.7 \cdot 10^{10} e^- (\equiv I_{\text{beam}} \approx 48.5 \text{ mA})$

accelerating frequency $f_{\text{RF}} = 714 \text{ MHz}$

revolution frequency $f_{\text{rev}} = f_{\text{RF}} / 330 = 2.1636 \text{ MHz} (\equiv t_{\text{rev}} = 462.18 \text{ ns})$

bunch spacing $t_{\text{bunch}} = t_{\text{RF}} / 2 = 2.8011 \text{ ns}$

batch spacing $t_{\text{batch}} = t_{\text{rev}} / 3 = 154.06 \text{ ns}$

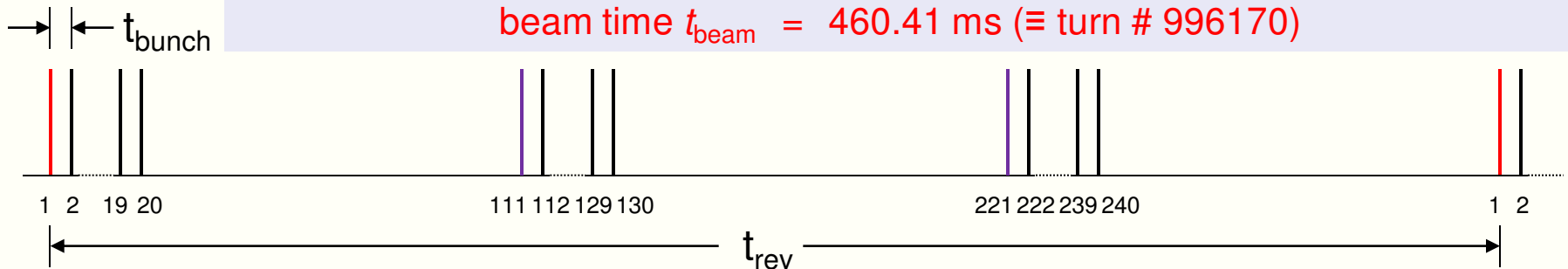
horizontal betatron tune $\approx 15.204 (\equiv f_h \approx 441 \text{ kHz})$

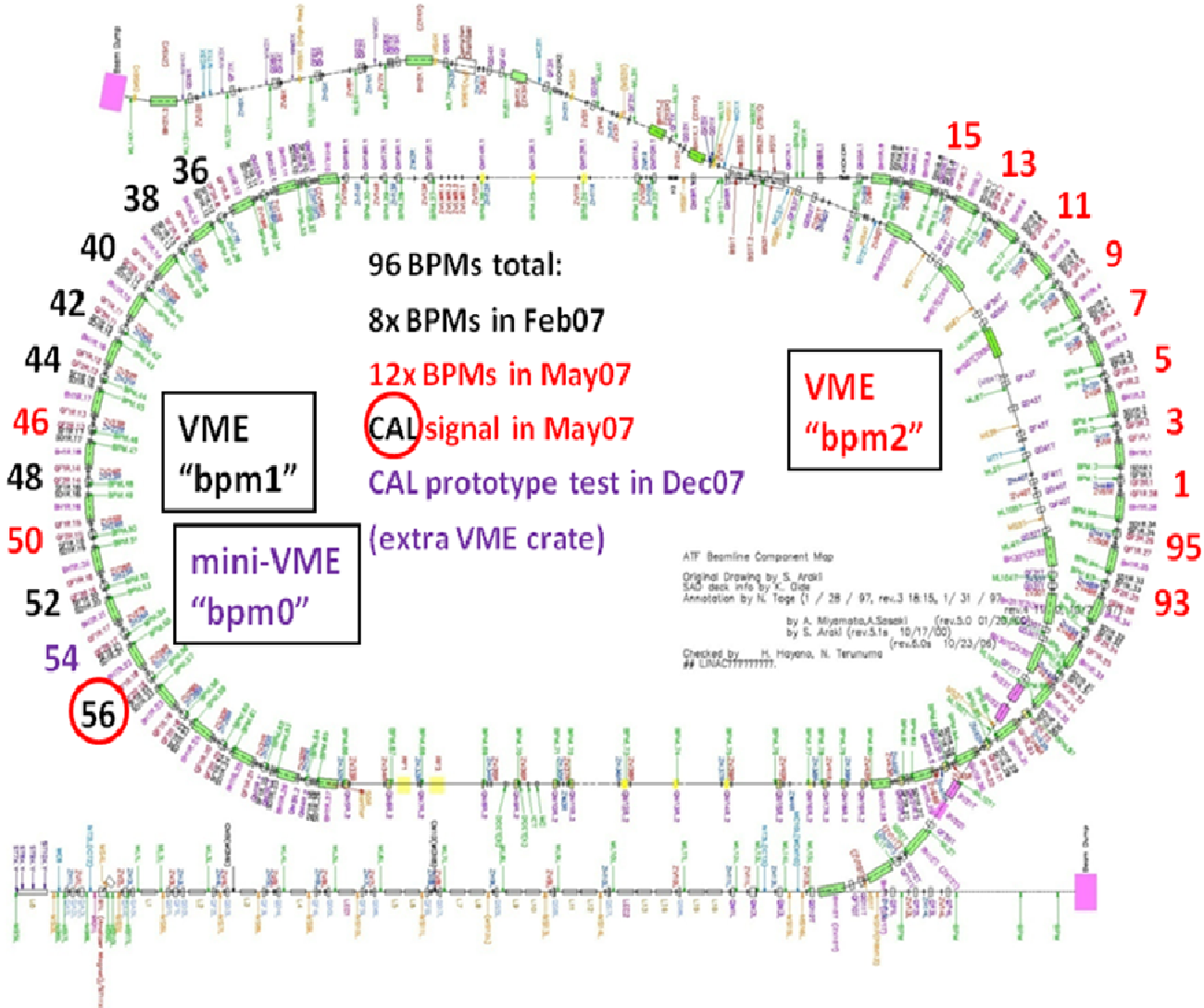
vertical betatron tune $\approx 8.462 (\equiv f_v \approx 1000 \text{ kHz})$

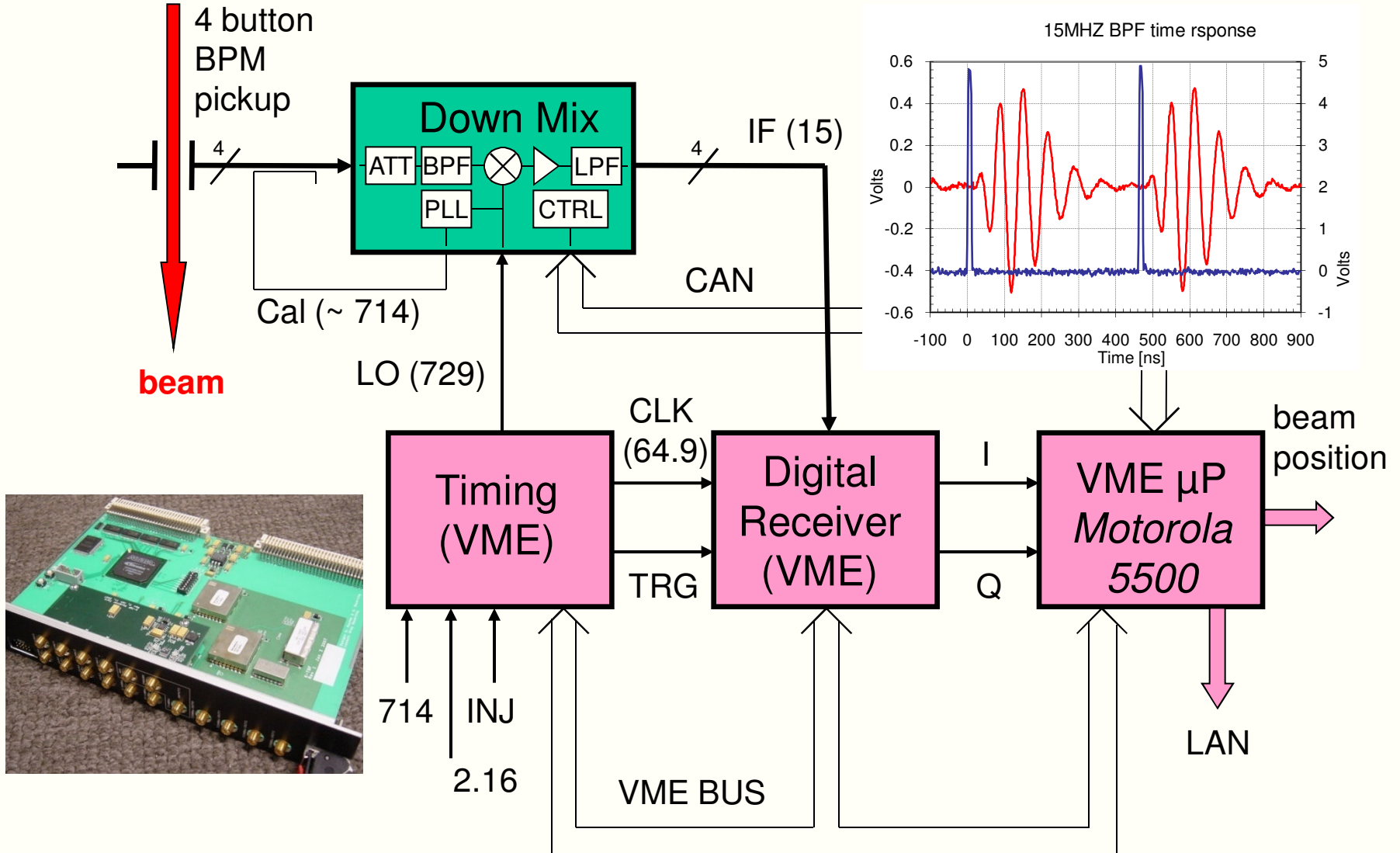
synchrotron tune $\approx 0.0045 (\equiv f_s \approx 9.7 \text{ kHz})$

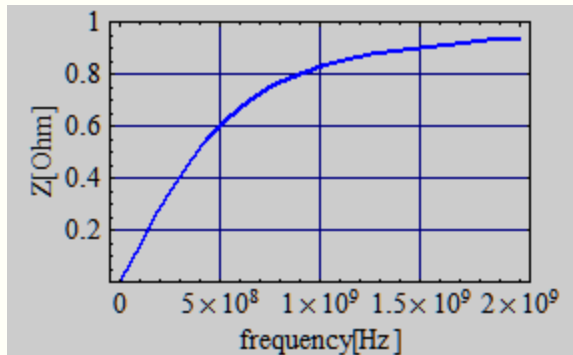
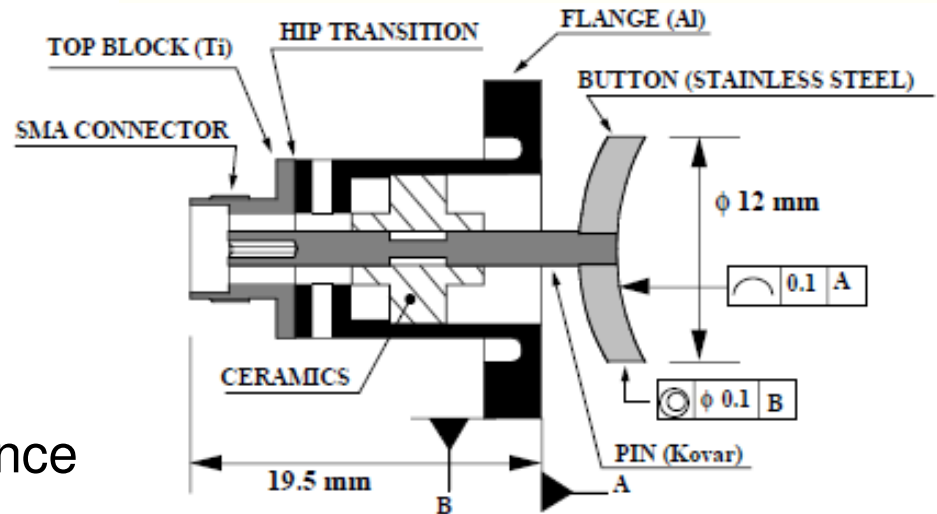
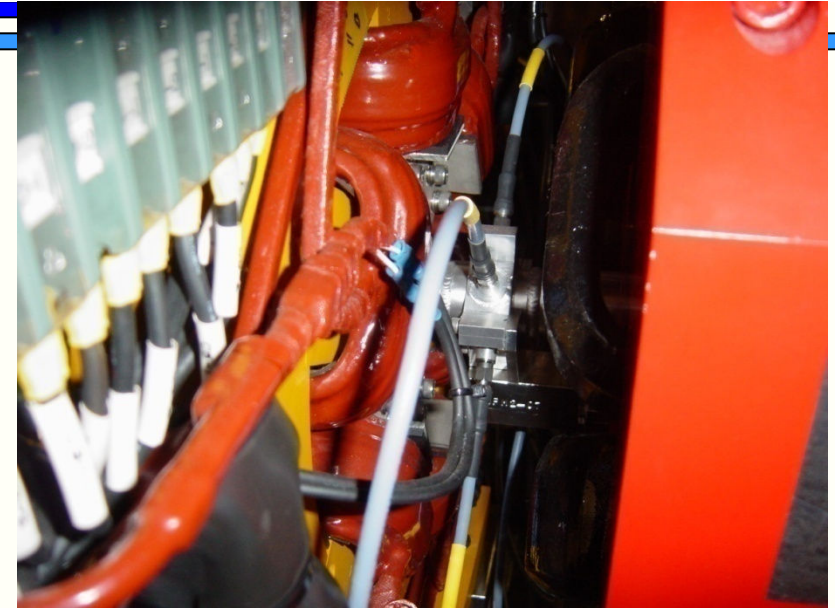
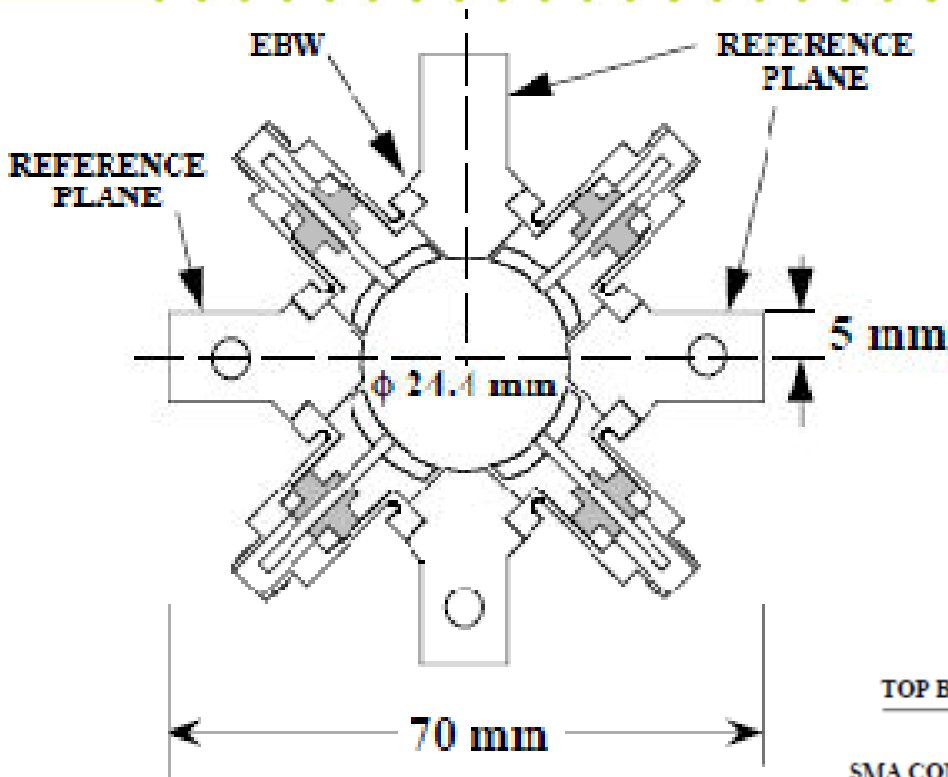
repetition frequency $f_{\text{rep}} = 1.56 \text{ Hz} (\equiv t_{\text{rep}} = 640 \text{ ms})$

beam time $t_{\text{beam}} = 460.41 \text{ ms} (\equiv \text{turn \# } 996170)$



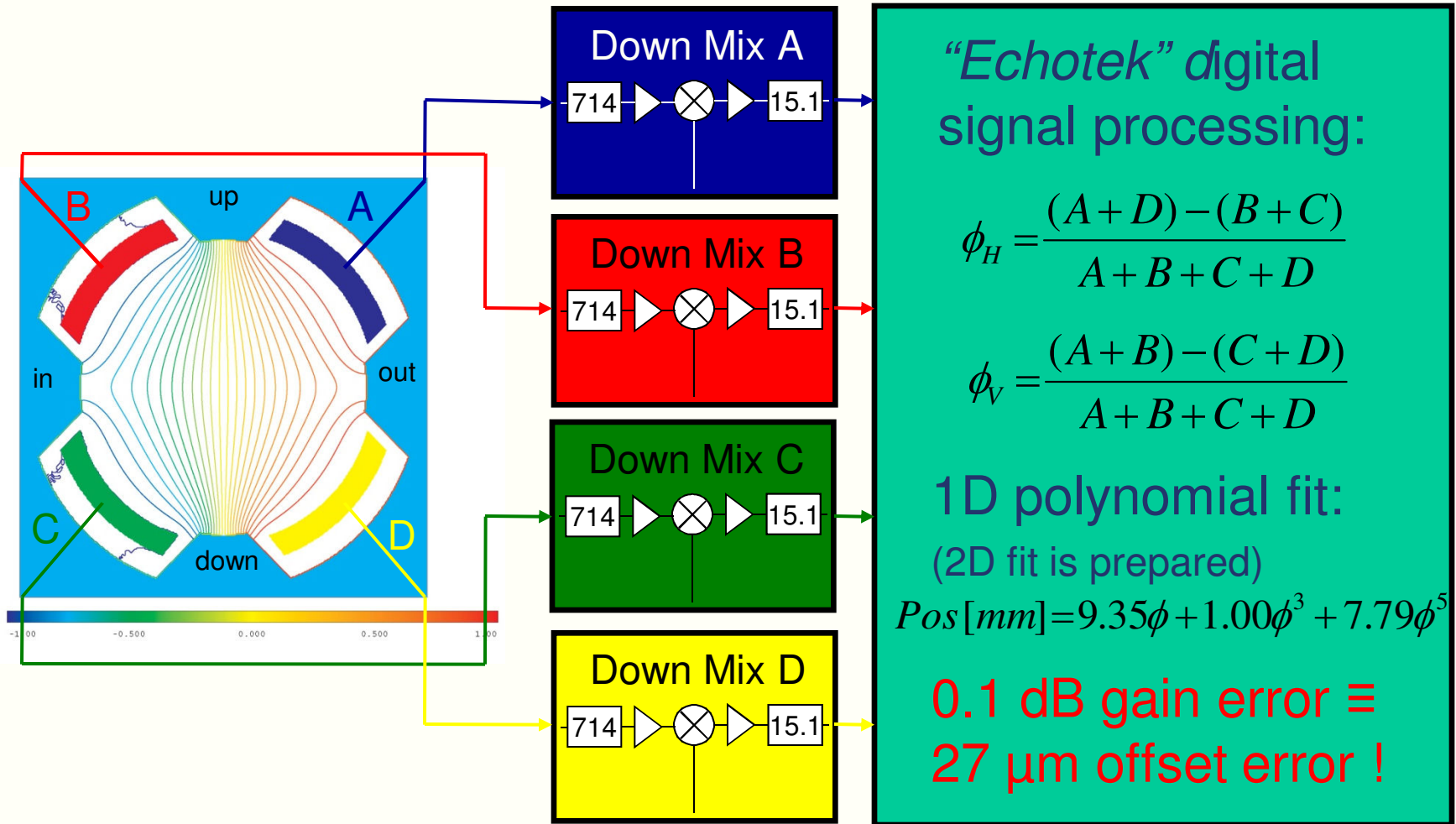


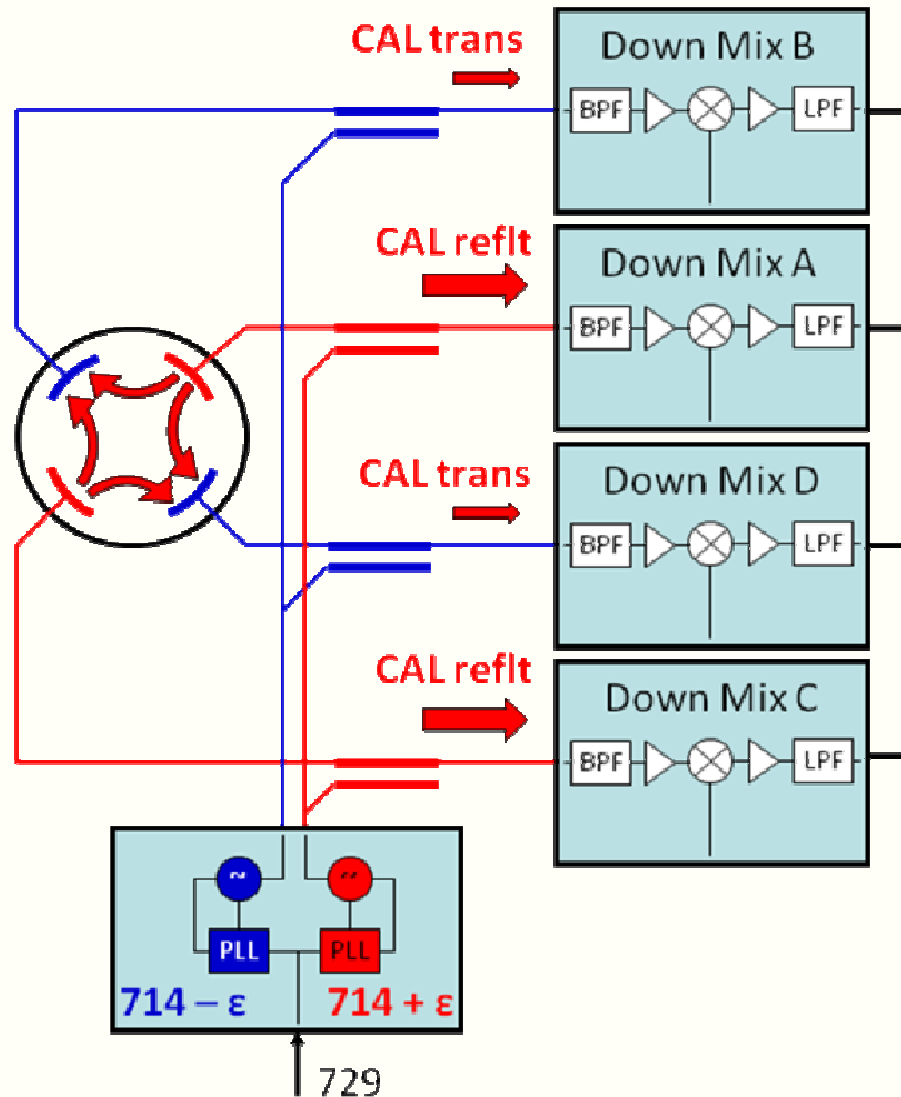




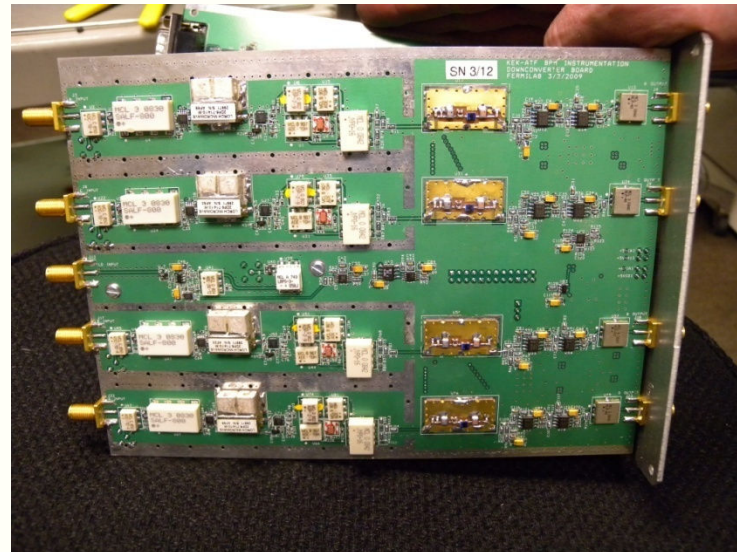
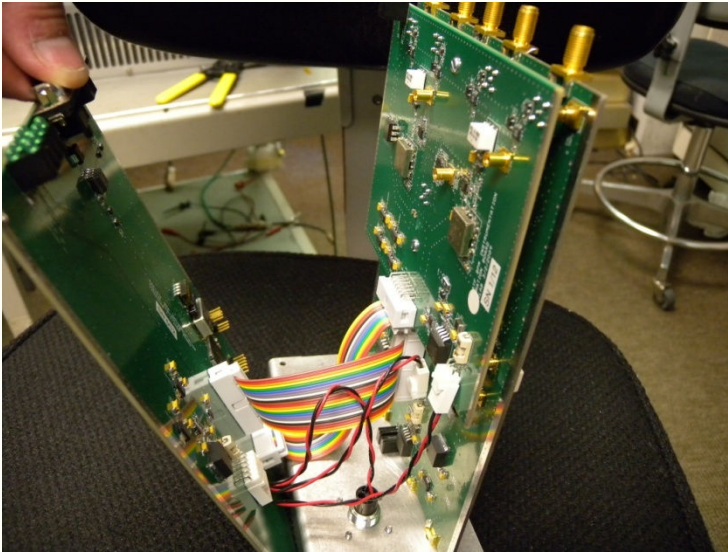
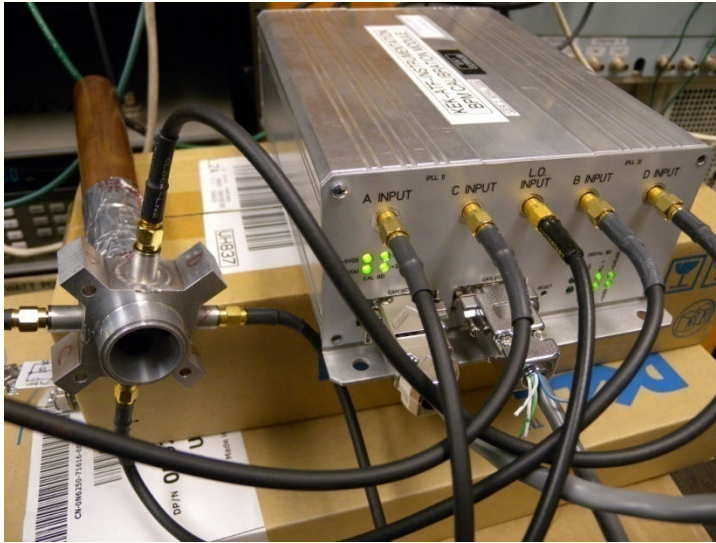
Button:
transfer
impedance

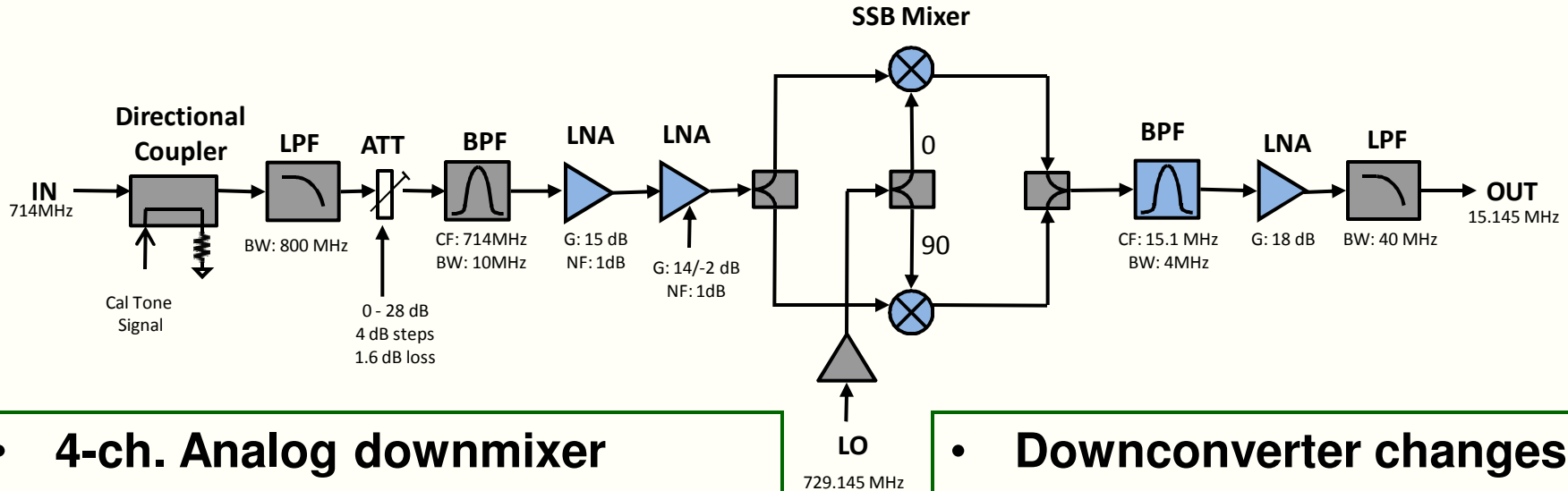
Beam Position Signal Processing





- **2 calibration tones:**
 - $714 + \epsilon$ MHz
 - $714 - \epsilon$ MHz
 - In passband of the downconverter
 - Coupled through the button BPM
 - Alternative: Reflected CAL signal
- **On-line calibration**
 - In presents of beam signals
 - Available only in narrowband mode
 - Need separate downconverter channels

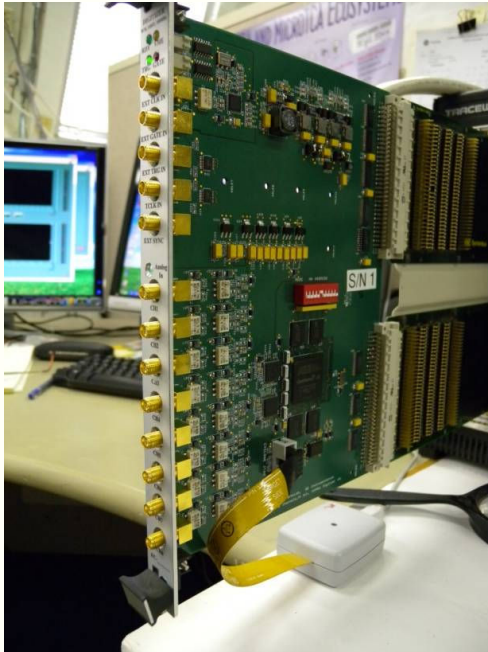




- **4-ch. Analog downmixer**
 - IN: 714, LO: 729.1, IF: 15.1 MHz
 - CAN-bus controlled gain, attenuator & cal system
 - Gain switchable, low-noise, high IP3 input gain stage
 - Image rejection (SSB) mixer
 - ~30 dB gain, ultralinear IF stage

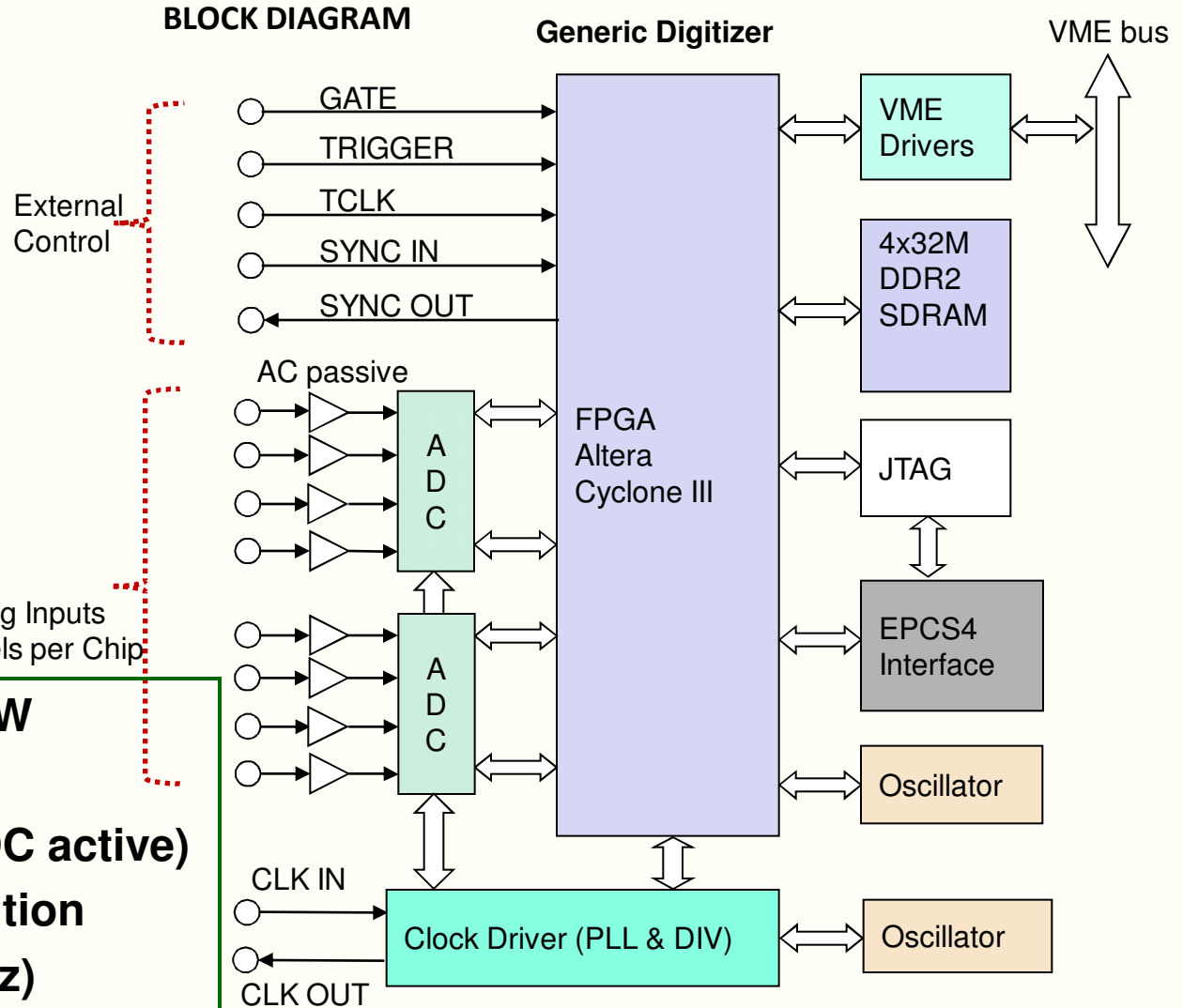
- **Downconverter changes**
 - Change the gain distribution (RF+, IF-)
 - Change mixers (+17 dBm -> +13 dBm)
 - Change response of the IF section BPF

8-Ch, 14-bit, 125 MS/s VME Digitizer

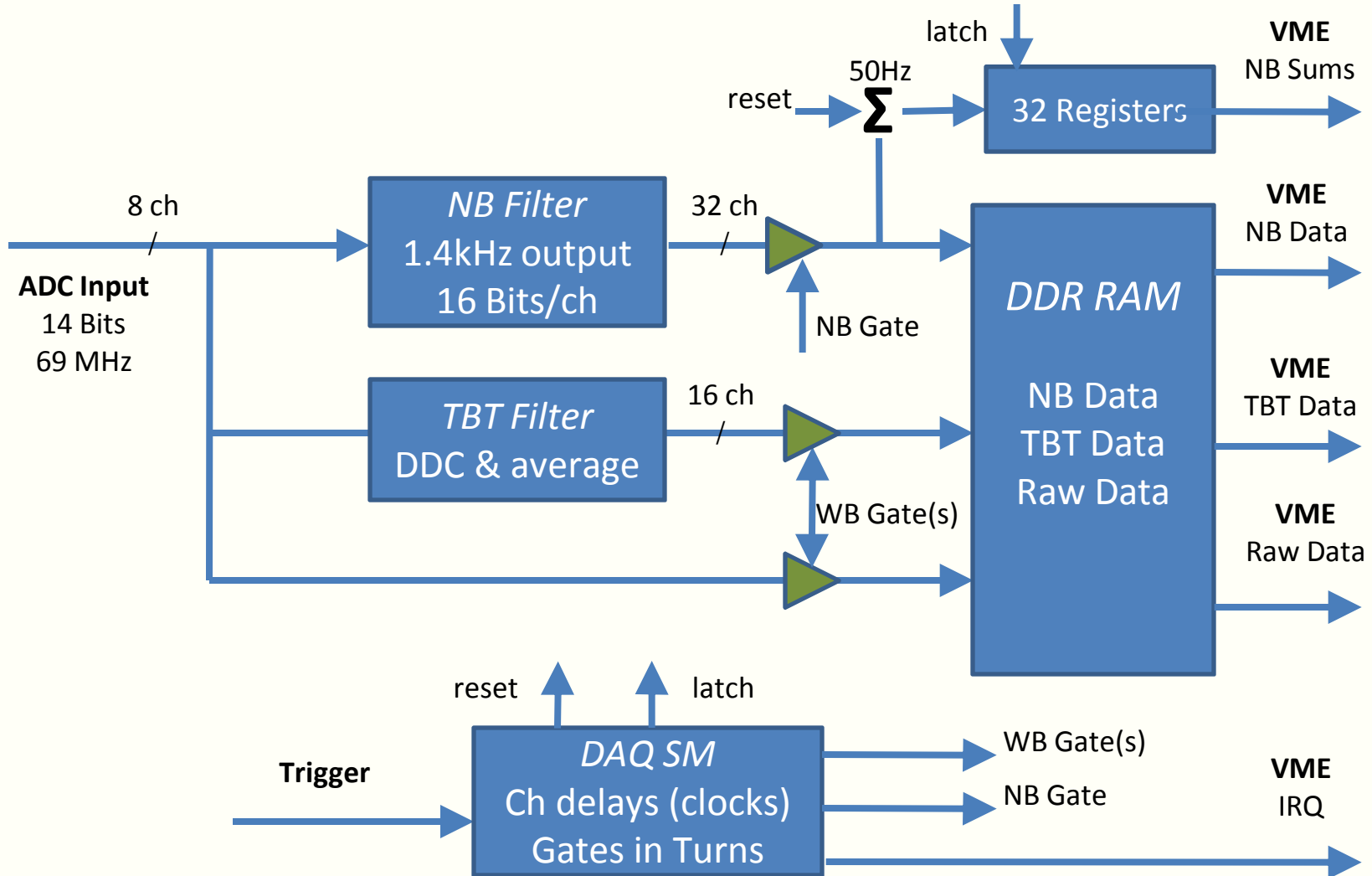


8 Analog Inputs
4 Channels per Chip

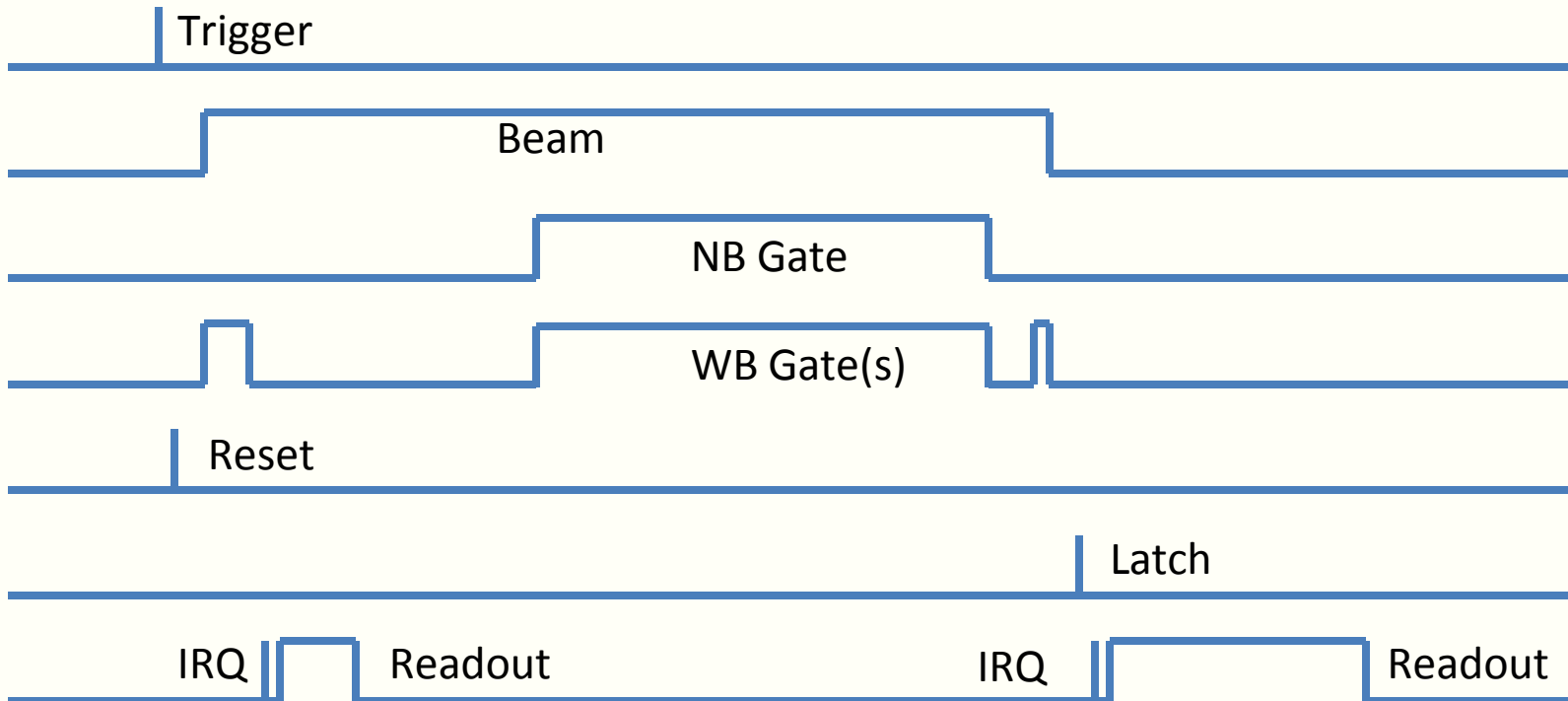
- 125 MSPS, 500 MHz BW
- 4-ch serial ADC chips
- 8-ch, AC passive (or DC active)
- PLL/VCO CLK distribution
- SNR > 72 dB (@50 MHz)



- **No Modes** - one external trigger processes data
 - Raw data to RAM
 - TBT readback & process (DDC & average) -> I,Q per turn
 - diagnostic readback
 - Narrowband processing (Filter & Decimate)
 - Store array of I,Q per channel for readback
 - Provide single sum I,Q per channel over $n \cdot 50$ Hz
 - Programmable trigger delay per channel (adc samples)
- Any data type (NB, TBT, Raw) can be readback after each trigger
 - All data will be read out as I,Q pairs
 - **Caveat: The CAL tone has to be disabled for TBT data**
 - Each board will pull IRQs when data is ready

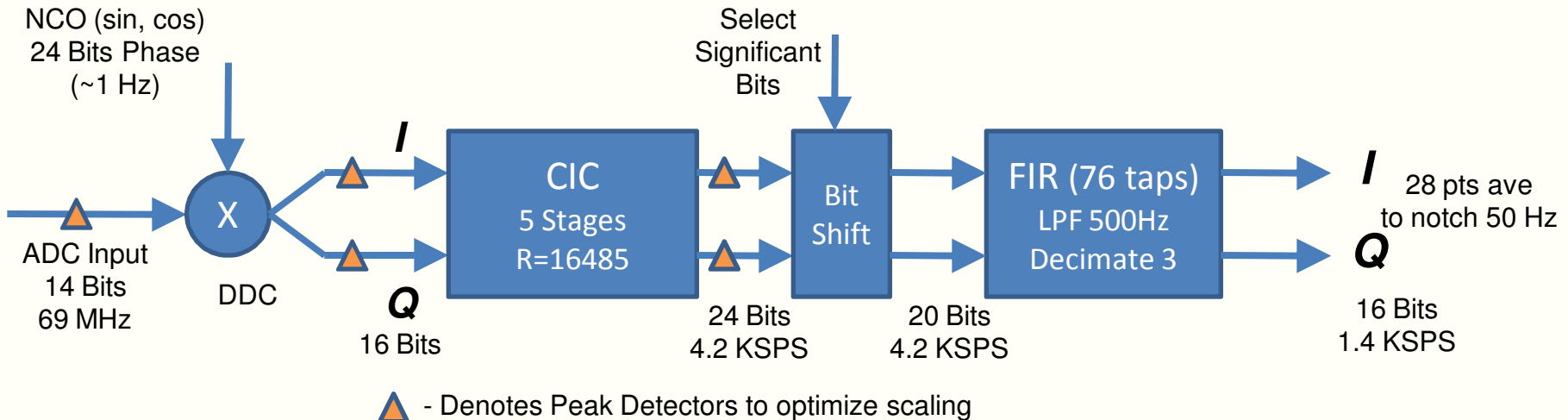


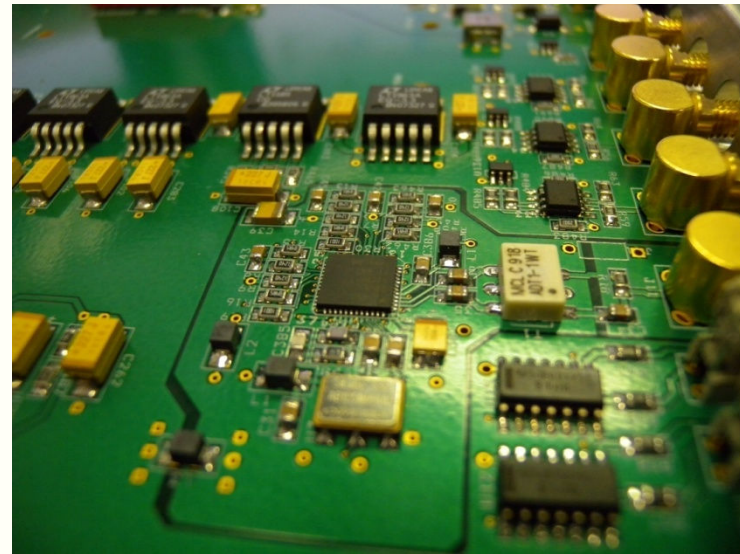
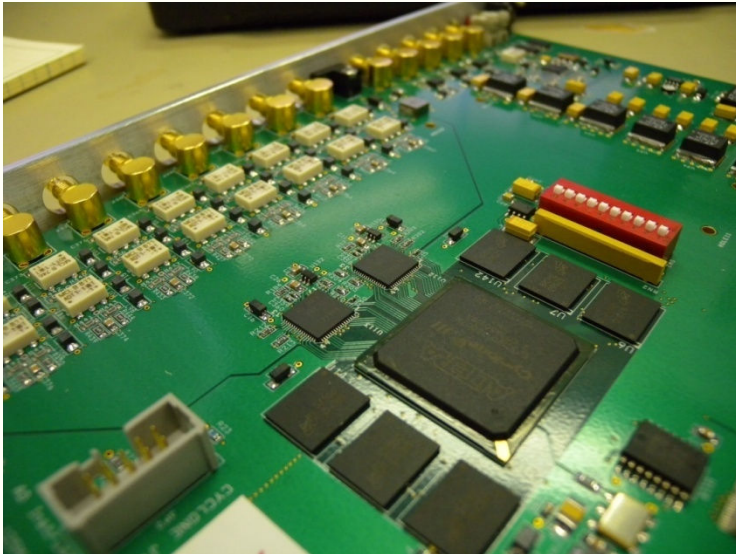
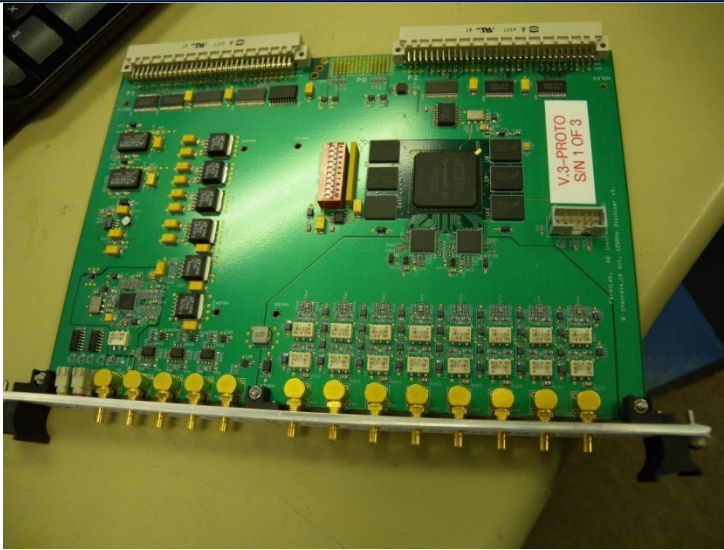
- Trigger before beam injection (injection rep rate is ~ 1.5 Hz)
 - Beam in machine for $\sim 1e6$ turns (~ 450 msec)
 - Each machine turn is 462.18 nsec \rightarrow 32 ADC clocks
 - Gates specified in turns (need to account for filter delay/decimation for NB)
 - Data in boards is overwritten on each trigger
 - Note for WB readback (diagnostic and some TBT data) it will be necessary to halt the system to readback all data over the network - *these are special study modes*

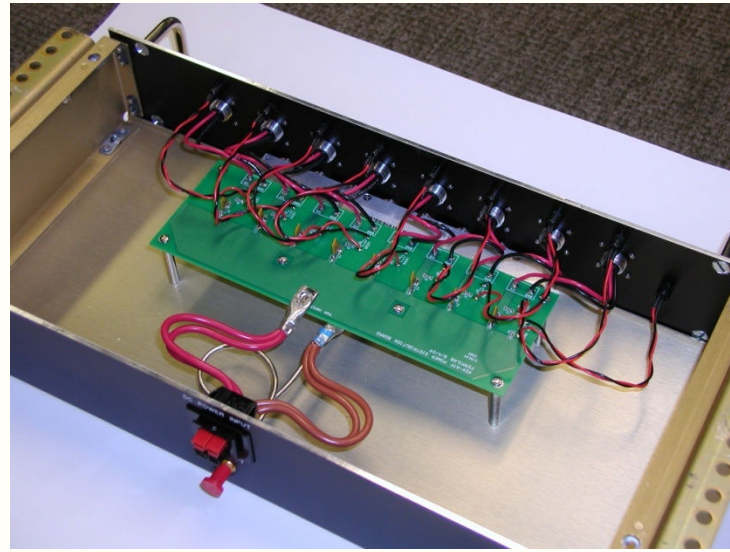
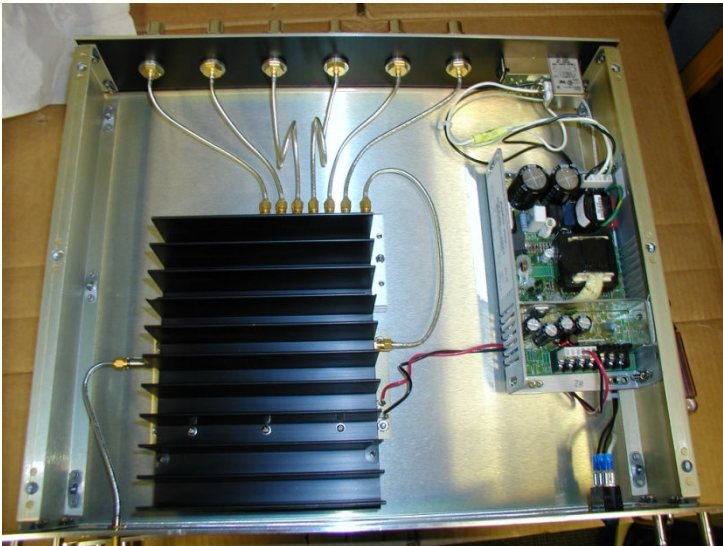
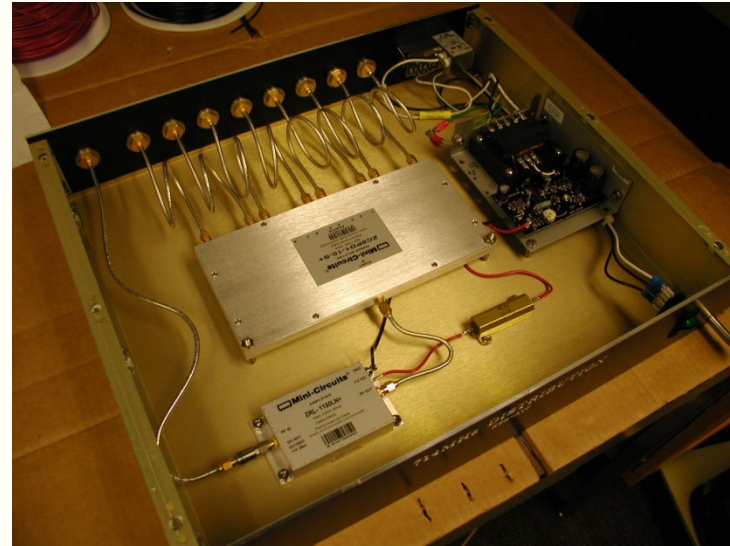


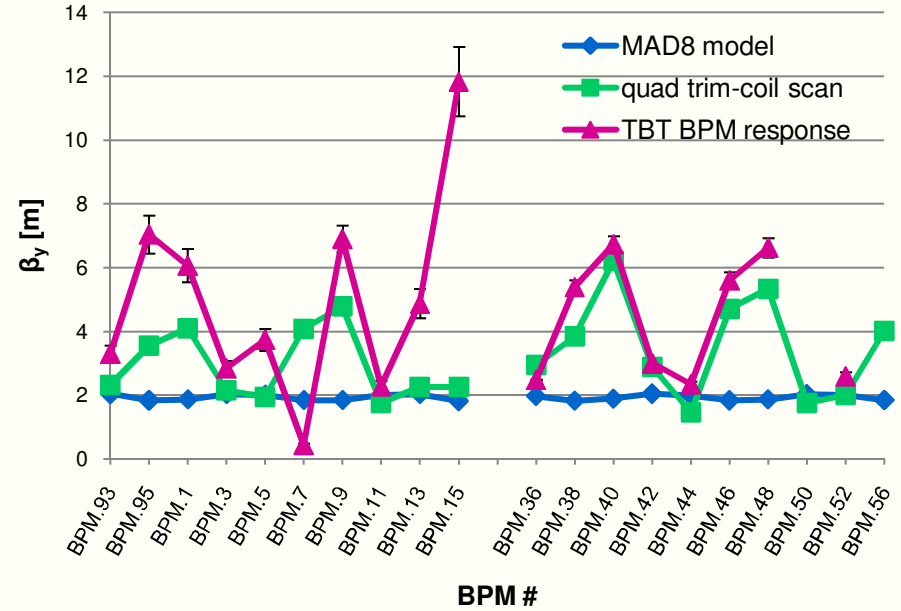
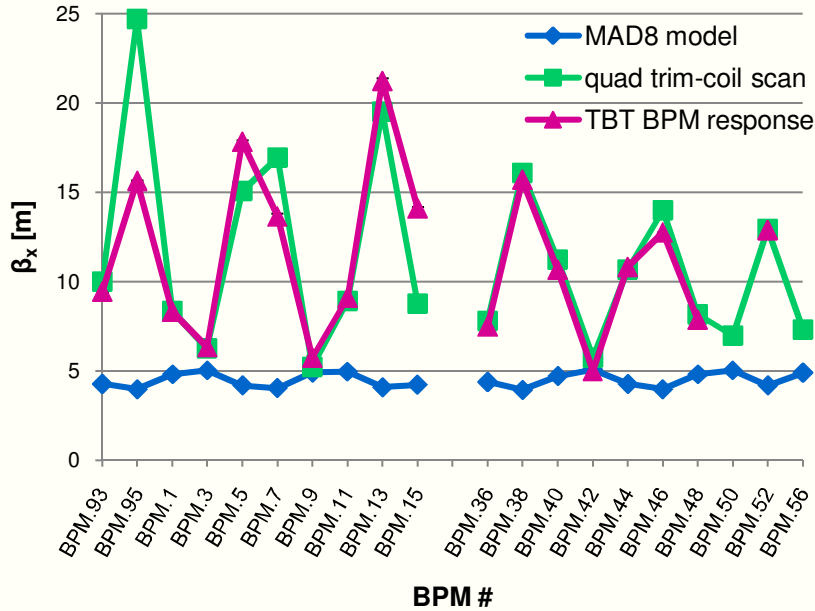
- **Design footprint for 8 ADC channels**
 - 2 NCOs for beam and cal frequencies
-> 16 DDCs
 - 32 CIC Filters operating at 69 MHz
 - 5 stage CIC uses 13 k LEs and <1% of RAM
 - 1 Serial FIR Filter will process all 32 CIC Filter outputs
 - 76 tap FIR (400 Hz BW, 500 Hz Stop, -120 db stopband)
 - Decimate by 3 to 1.4 KSPS output

- **General Design Considerations**
 - For 256 pts get 183 msec data points
 - *I,Q* will be read out and magnitude/position calculations done in the VME CPU
 - Raw *I,Q* Data is stored in DDR Ram and may be readback for detailed orbit analysis
 - Provide average in realtime for single *I,Q* readback
 - Average a multiple of 28 to remove 50Hz



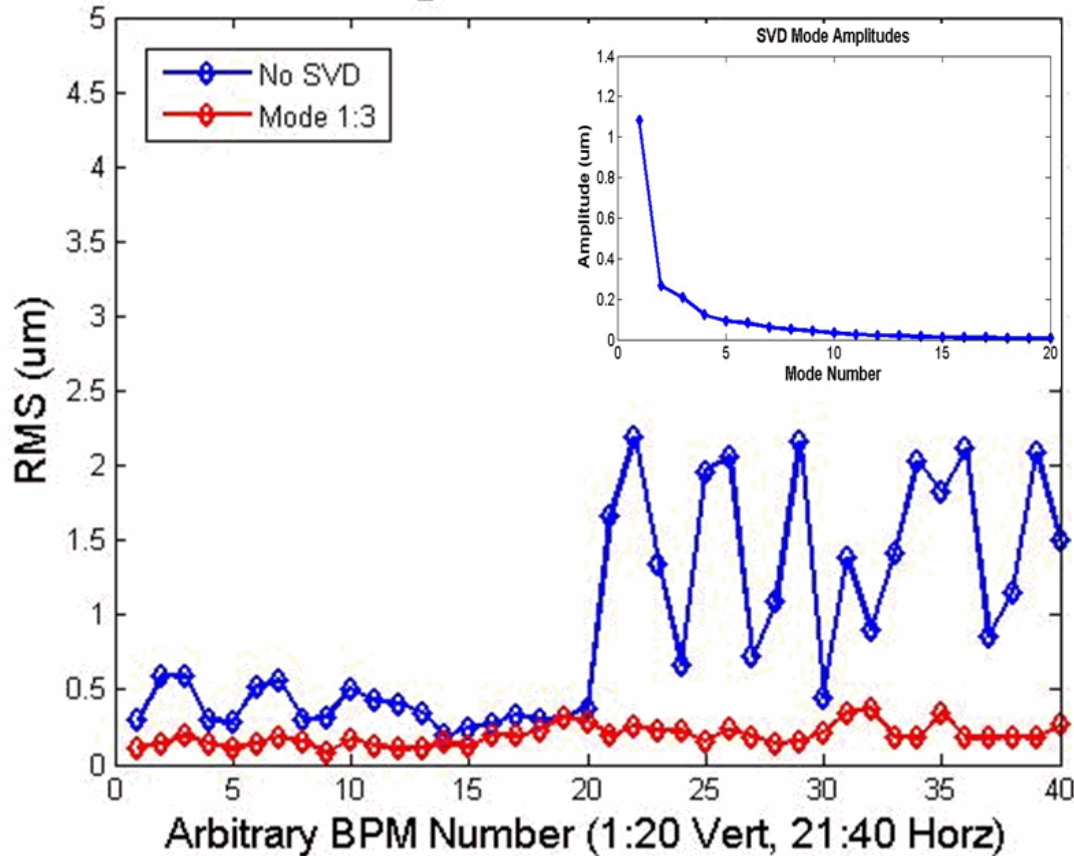






- MAD8 model (M. Woodley, marginal differences wrt. Kuroda SAD model).
- Nearby quadrupole trim coil scan (May 2008).
- TBT Fourier analysis, amplitude by fit to beta measured through trim coil scan (April 2008).

Single Shot BPM RMS



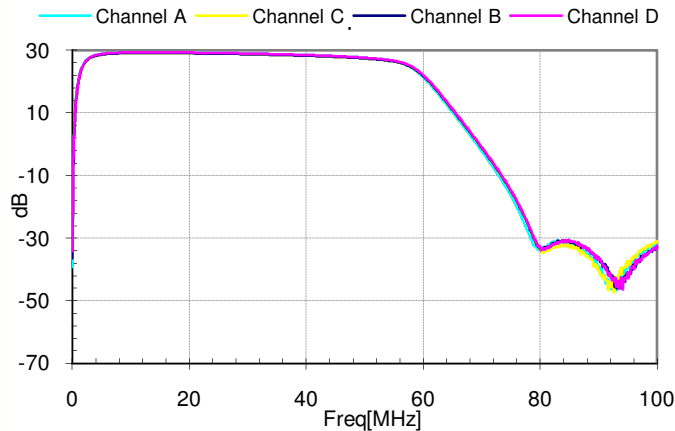
- Triggered at turn #500,000
- ~200 ms position data per shot (1280 narrowband mode BPM measurements).
- 126 tap box car filter to reject 50 Hz:
 - ~ 800 nm resolution
- SVD analysis, removing modes with hor./ vert. correlation:
 - ~200 nm resolution

- **After 4 years of developments and beam studies the ATF damping ring BPM upgrade enters the final lap:**
 - **A tailored BPM system towards the specific needs of the ATF damping ring has been developed:**
 - no DAC outputs, analog downconversion in the tunnel, digitalization in the 1st Nyquist passband, automatic calibration system, adaptable design (attenuators, mod. FPGA & EPICS codes)
 - **The hardware design is frozen**
 - Successful prototype testing of every system module completed.
 - All electronics hardware components are in house.
 - Assembly is underway, followed by individual tests and an integrated system test.
 - **Next Steps:**
 - Installation and commissioning of the system (May 2010).
 - First beam studies with the new BPM system.

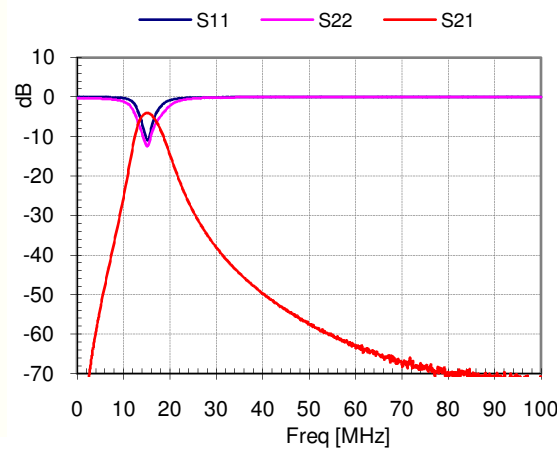


- New read-out hard-, firm- and software, BPM pickups (button-style) stay unchanged.
- R&D activities over the last couple of years on 20 BPMs in the arcs, utilizing mixed analog/digital signal processing
 - Test of different analog downconverters (w/o CAL)
 - Digital signal processing based on spare *Echotek* digital receivers.
- Final upgrade scenario (96 BPMs, plus spares)
 - 714-to-15.1 MHz analog downconverter with CAN-bus controlled calibration tone, located in the tunnel.
 - VME hard- & software, in 4 rack locations
 - 8-ch. 125 MSPS digitizer with an *Altera Cyclone III* FPGA
 - 12 ch. VME timing generator (Fermilab).
 - *Motorola 5500* VME controller, with CAN-bus interface, running *VxWorks* & *EPICS* software
 - Auxiliary hardware, e.g. power supplies and distribution, LO-signal distribution, CAN-bus distribution, etc.

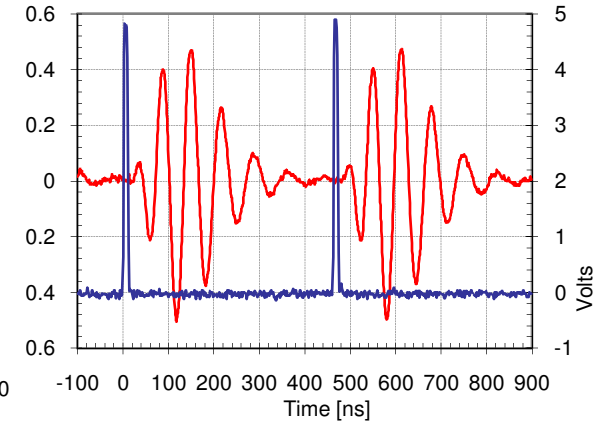
KEK-ATF-09 Downconverter BD IF section



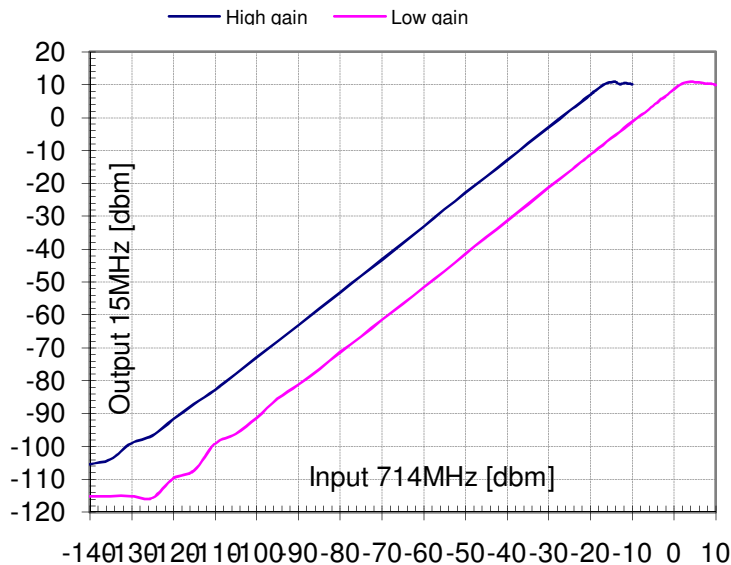
KEK-ATF 15MHz BPF frequency



15MHz BPF time response



ATF_KEK Downconverter dynamic range test



- **Modified IF section**
 - Low-noise gain stage
 - 15.1±1.5 MHz BPF, ~400 ns ring-time
- **Improved NF & dynamic range**
 - NF = 17 dB (?)
 - >90 dB dynamic range

- **Control Space**

- Channel delays (8)
0 to 31 samples
- Gate parameters (18)
1 to ~1e6 turns
 - NB specified by start and stop turn
 - WB (8 gates) specified by start and stop turn
- NCO frequencies (2), CIC shift (1)
 - Possibly FIR coefficients for NB
- Specify TBT box filter –
1st sample, number to average (2)
- IRQ Level (1)
 - Multi-level IRQ handler
 - Data Ready/Overflows
- Diagnostic Peak Detectors (to monitor saturation) each 32 bit register
 - Peak Detectors record max value at each stage for last injection (Reset & Latch from DAQ SM)

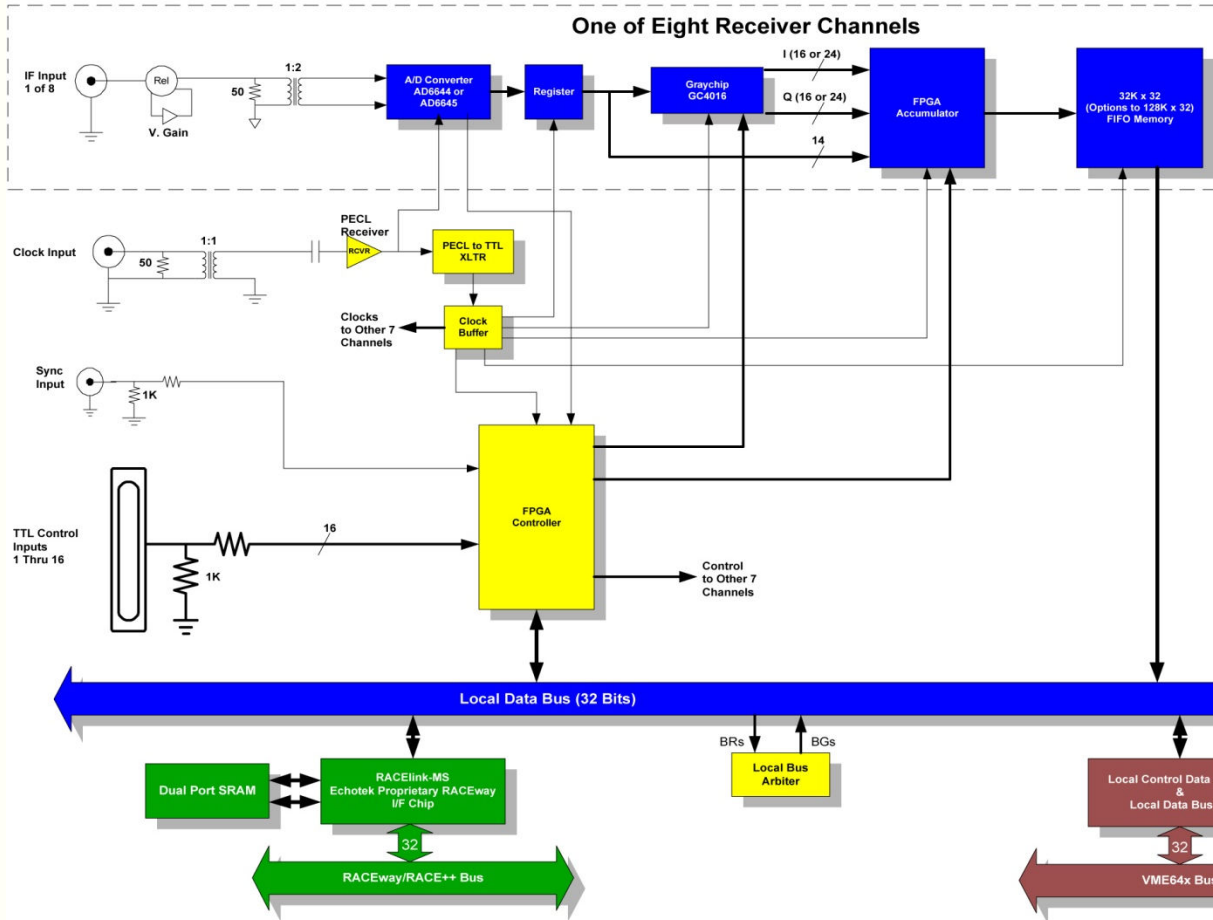
- **Store SumI, SumQ for each I,Q channel in 32 contiguous registers**

- Sum will be a multiple of 50 Hz (28 pts out of NB)
- Standard Narrowband readout

- **DDR RAM**

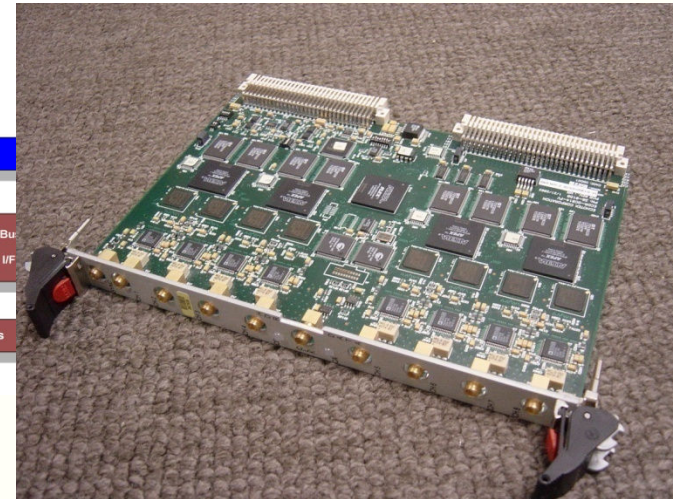
- All Data from gates stored in RAM
- Separate Banks for Narrowband, TBT, and RAW Data
 - Each Bank mapped to VME
 - Address offsets for each bank programmable
- Channel data in each bank can be readback as contiguous data blocks
 - Facilitate readback of data from single bpm if requested (ie TBT data)

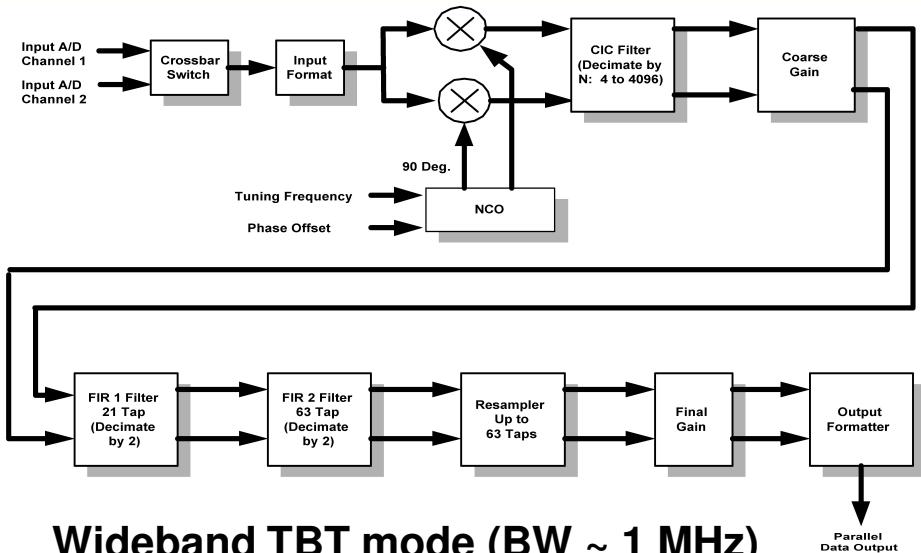
ECDR-GC814 BLOCK DIAGRAM



• **Echotek digital receiver**

- 8-ch VME64x module
- *Analog Devices* 14-bit 105 MS/s AD6645
- Each ADC channel: *Texas Instruments* 4-ch GC4016 “*Graychip*” digital downconverter
- 128 kWord FIFO





- **Graychip digital downconverter**
 - 4 independent channels per ADC
 - NCO set to $f_{IF} = 15.145$ MHz (downconvert to DC baseband)
 - ADC clock set to 32 samples per revolution: $f_{CLK} = 32 \times f_{rev} = 69.2$ MHz
 - Decimation and filtering for wide- and narrowband mode using CIC and FIR digital filters
 - Simultaneous DDC operation of beam and calibration signals!

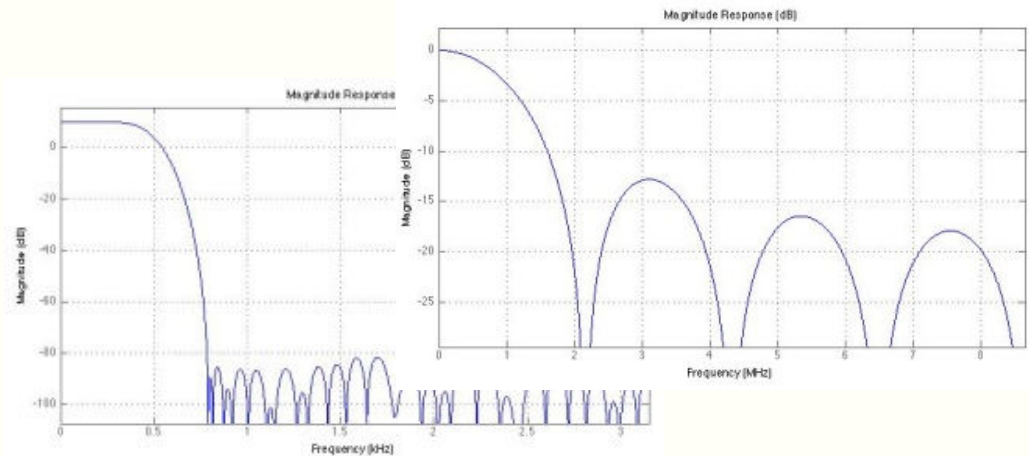
- **Wideband TBT mode (BW ~ 1 MHz)**

- 5 stage CIC: decimate by 4
- CFIR: 7-tap boxcar, decimate by 2
- PFIR 1-tap, no decimation

- **Narrowband mode (BW ~ 500 Hz),**

$t_{dec} = 158.7 \mu s, 1280$ pt (~200 ms)

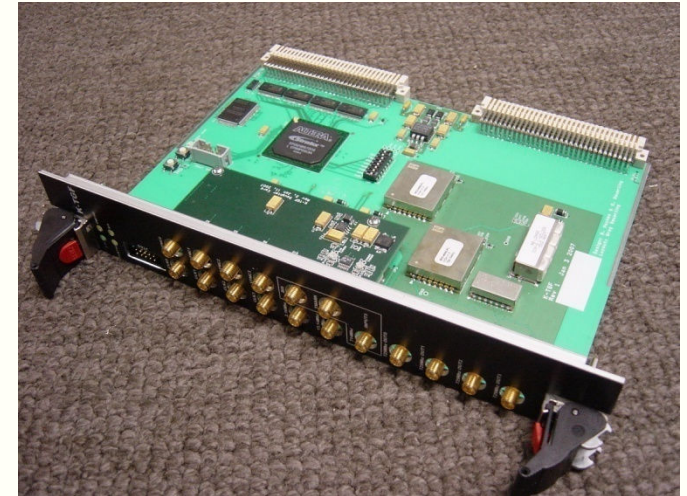
- 5 stage CIC: decimate by 2746
- CFIR: 21-tap RRC, decimate by 2
- PFIR: 63-tap RRC, decimate by 2



NB mode PFIR response

WB CFIR response

- **VME Timing module:**
 - $f_{\text{CLK}} = f_{\text{RF}} * 32/330 = 69.236$ MHz clock signals (4x)
 - $t_{\text{rev}} = 462.2$ ns turn marker signals (4x), 0...115 double-buckets (2.8 ns) delayable
 - To f_{RF} phase-locked $f_{\text{LO}} = 729.145$ MHz
 - Auxiliary f_{rev} and f_{IF} signals
- **Motorola 5500 VME CPU:**
 - Data collection and normalization
 - Box-car post-processing filter (20 ms)
 - Local diagnostic and control software
 - EPICS control interface
- **Calibration & remote control unit (prototype):**
 - To f_{RF} phase-locked $f_{\text{CAL}} \approx 714$ MHz (*Analog Devices ADF4153*)
 - In-passband, through button-BPM, or reflected signal calibration
 - 2nd and 3rd *Graychip* channels for CAL signal downconversion
 - CAN-bus remote control functions (attenuation, gain, PLL freq., etc.)



- **Calibration tone frequencies:**

- $f_{\text{CALx}} = 713.6 \text{ MHz}$

- $f_{\text{CALy}} = 714.4 \text{ MHz}$

- **Calibration procedure:**

- **Correction values:**

$$A_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4A_{\text{CAL}}}$$

$$B_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4B_{\text{CAL}}}$$

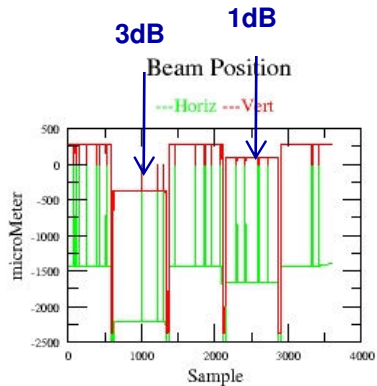
$$C_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4C_{\text{CAL}}}$$

$$D_{\text{Corr}} = \frac{A_{\text{CAL}} + B_{\text{CAL}} + C_{\text{CAL}} + D_{\text{CAL}}}{4D_{\text{CAL}}}$$

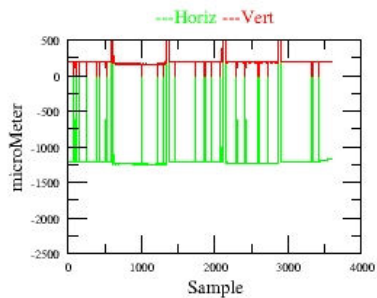
- **Corrected beam positions:**

$$\phi_{\text{Hcorr}} = \frac{(A A_{\text{Corr}} + D D_{\text{Corr}}) - (B B_{\text{Corr}} + C C_{\text{Corr}})}{A A_{\text{Corr}} + B B_{\text{Corr}} + C C_{\text{Corr}} + D D_{\text{Corr}}}$$

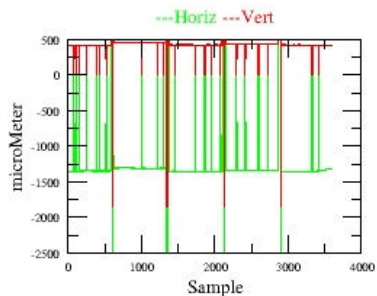
$$\phi_{\text{Vcorr}} = \frac{(A A_{\text{Corr}} + B B_{\text{Corr}}) - (C C_{\text{Corr}} + D D_{\text{Corr}})}{A A_{\text{Corr}} + B B_{\text{Corr}} + C C_{\text{Corr}} + D D_{\text{Corr}}}$$



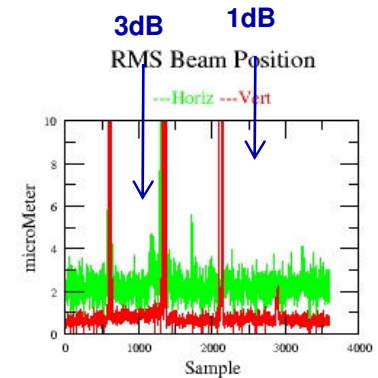
Coupled Position



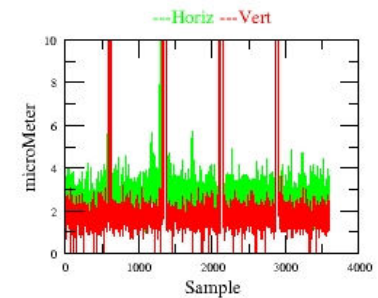
Reflected Position



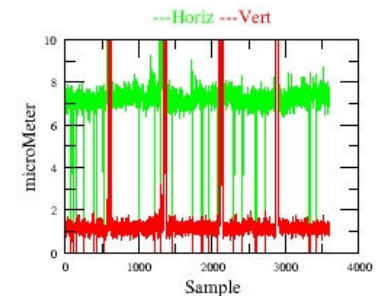
- Calibration on, datalogger on
- Comparing uncorrected, corrected (coupled-through), and corrected (reflected)
- Introduce large 3 & 1 dB gain errors.
- Automatic correction compensates the gain error almost completely!!
- Corrected beam position shows a slight increase of the RMS error (to be further studies!).

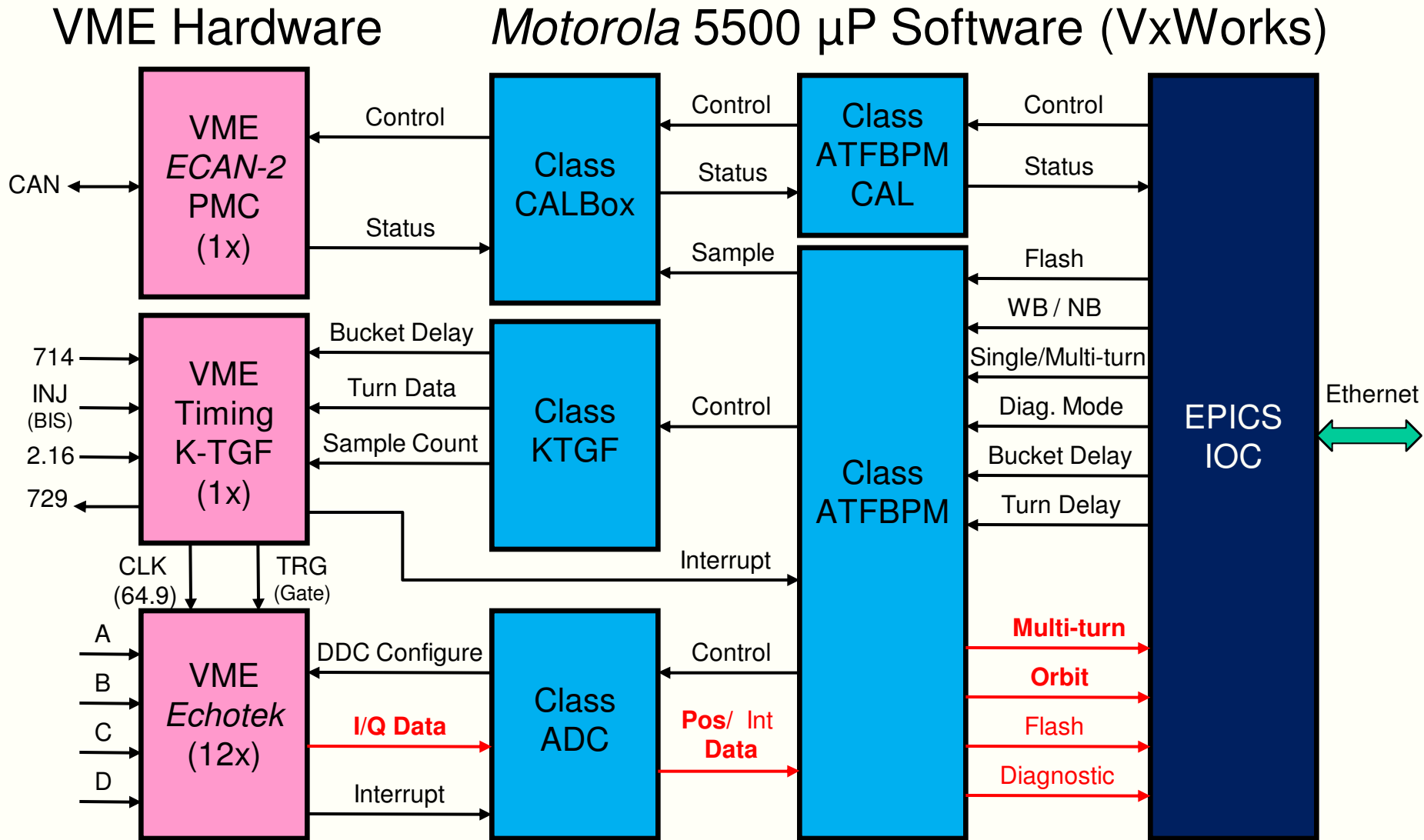


RMS Coupled Position

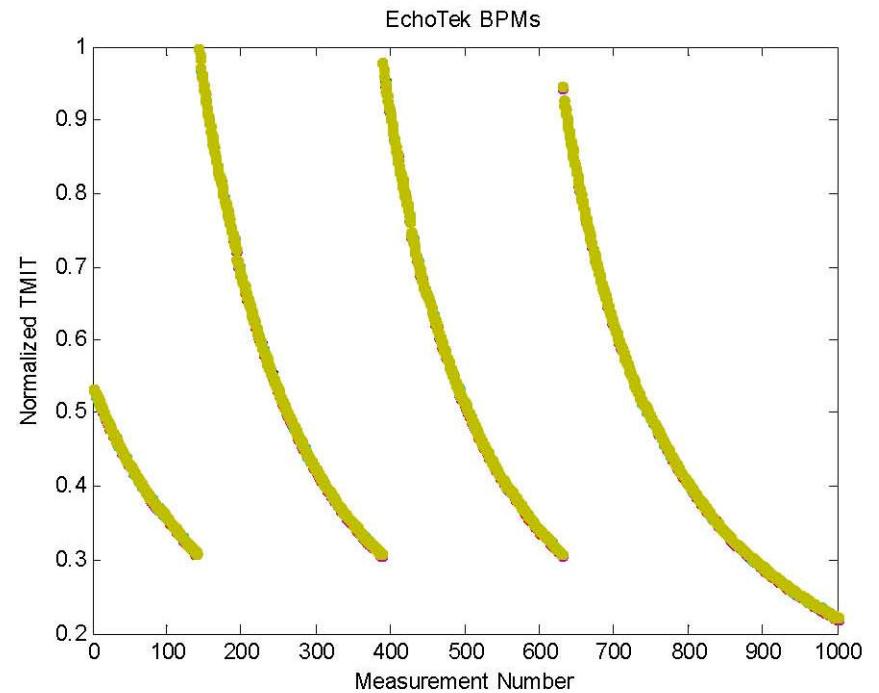
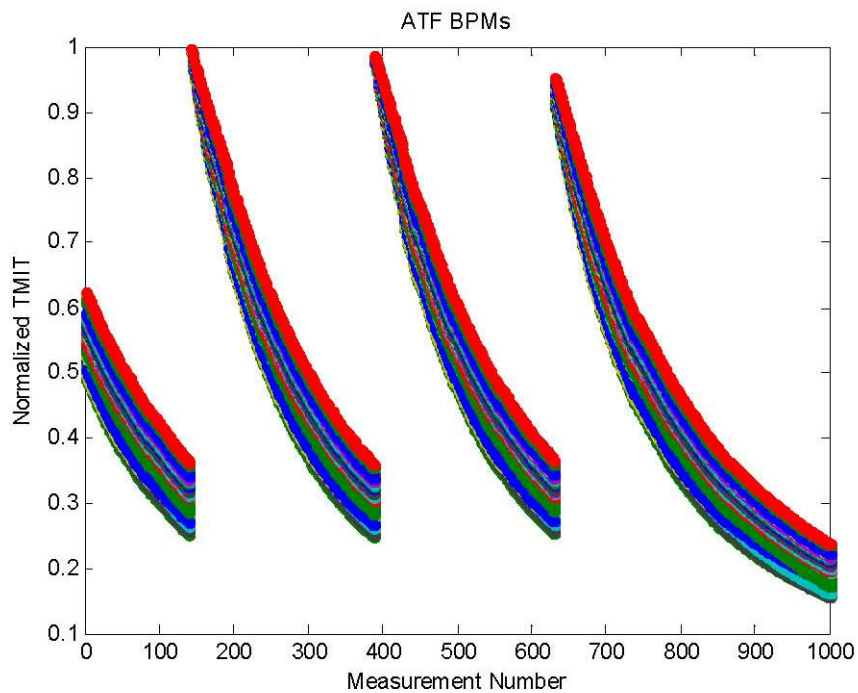


RMS Reflected Position



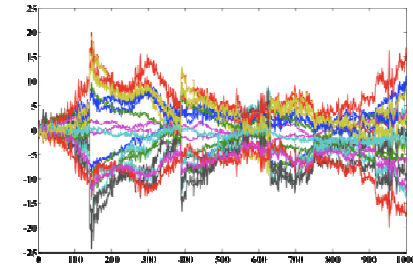
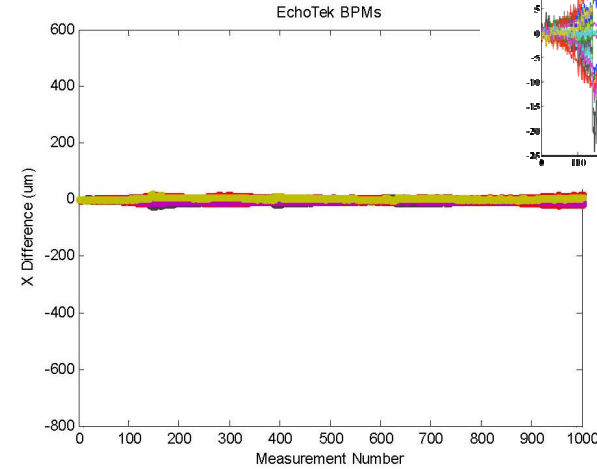
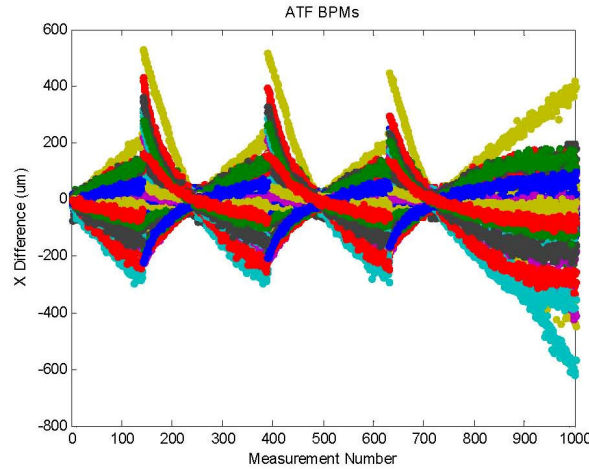


Normalized Intensities



Horizontal Position

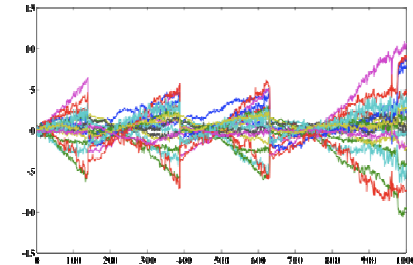
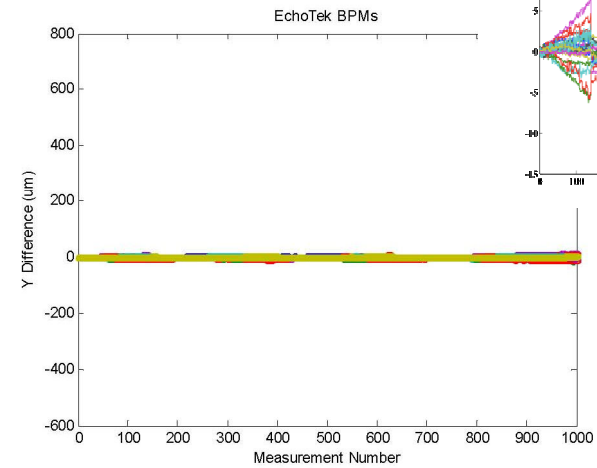
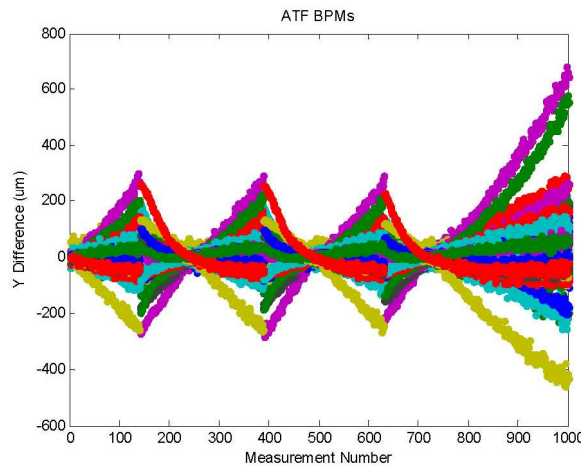
$\pm 700 \mu\text{m}$



$\pm 25 \mu\text{m}$

Vertical Position

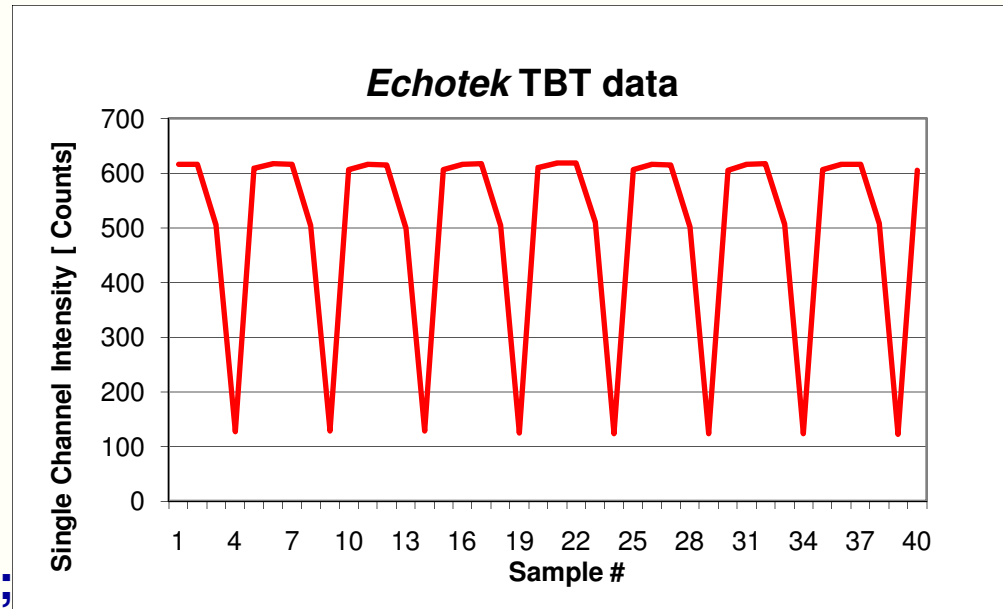
$\pm 700 \mu\text{m}$



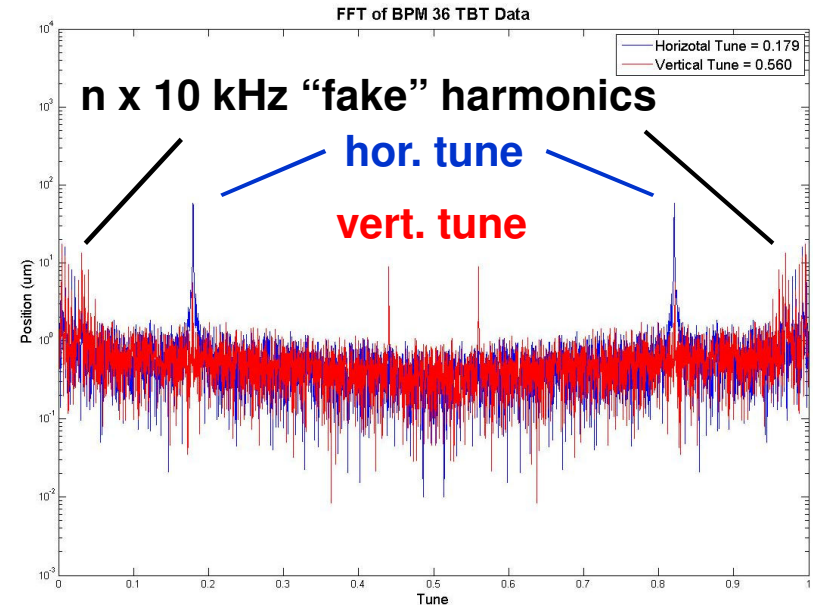
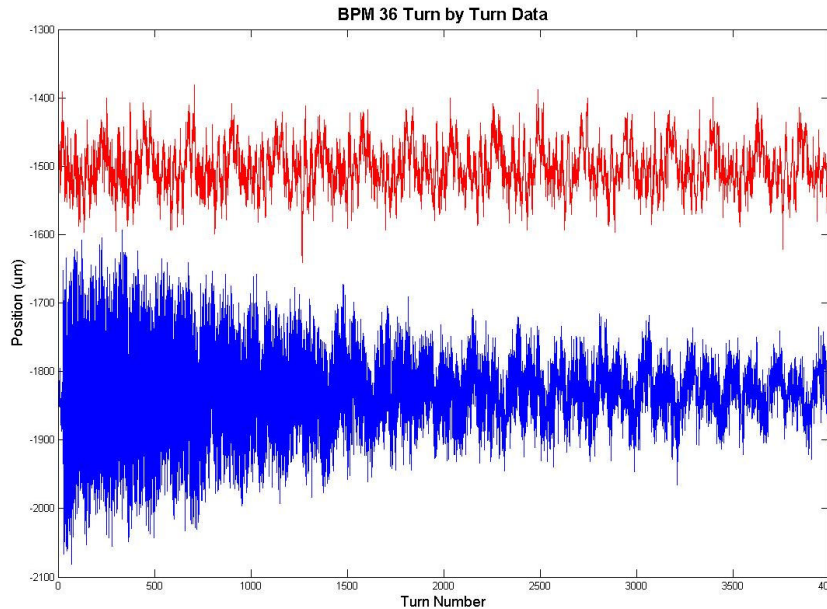
$\pm 15 \mu\text{m}$

- Several “issues” had to be resolved:

- CIC & FIR digital filter impulse responses to resolve true turn-by-turn data (no “smearing”)
- Timing issues, e.g. channel-to-channel, as well as between BPMs and “houses” (VME crates); and of course the usual “seam” problem.



- In particular for the kicked beam TBT response tests:
 - Vertical beta at pinger is 0.5 m (12 times smaller than the horizontal one): we had to resort to injection oscillations -> lower resolution.



- Turn-by-Turn data BPM #36 (pinger: On)
- Identifying hor. and vert. tune lines (387 kHz, 1.212 MHz).
- Observed short time, broadband TBT resolution: few μm !
- **Observation of “fake” harmonics at $n \times 10$ kHz (not f_s), due to power supply EMI in the analog downconverter unit!**

- TBT data at the j^{th} BPM following a single kick in the z -plane ($z \equiv x, y$):

$$z_n^j = \frac{1}{2} \sqrt{\beta_z^j} e^{i\Phi_z^j} A_z e^{iQ_z(\theta_j + 2\pi n)} + c.c.$$

– with

$n \equiv$ turn number, $A_z = |A_z| e^{i\delta_z} \equiv$ constant of motion

$\Phi_z \equiv \mu_z - Q_z \theta$ (periodic phase function)

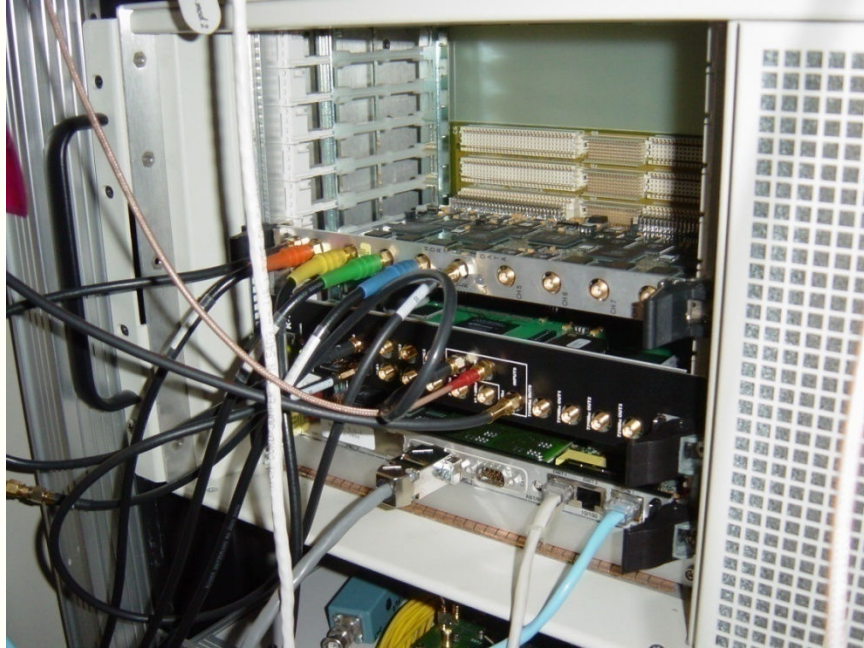
- Twiss functions:

$$\beta_z^j = |Z_j(Q_z)|^2 / |A_z|^2 \quad \mu_z^j = \arg(Z_j) - \delta_z$$

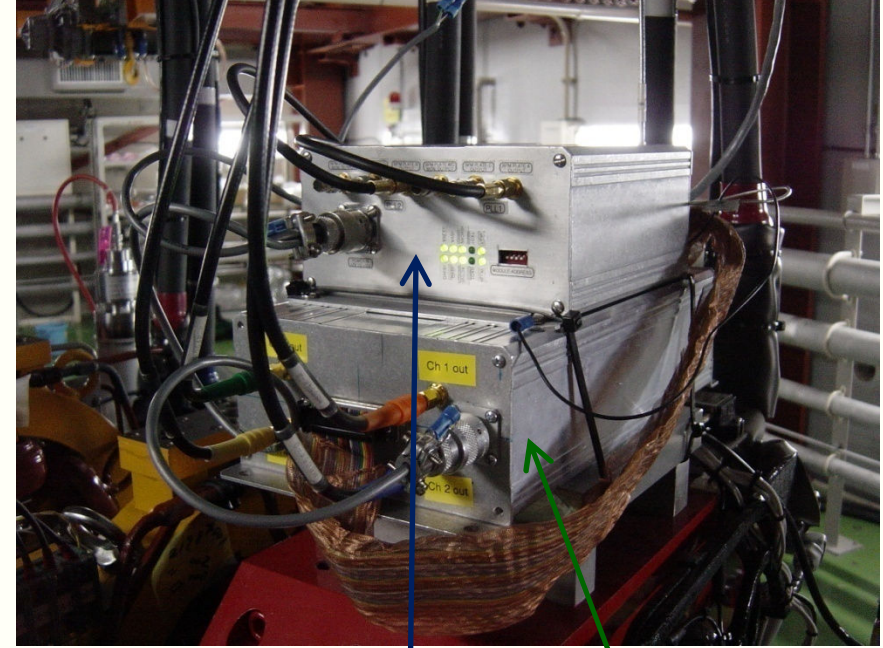
$Z_j(Q_z) \equiv$ Fourier component of z_j

- Amplitude fit:

$$|A_z|^2 = \frac{\sum_j 1/\beta_z^{0j}}{\sum_j 1/|Z_j(Q_z)|^2}$$

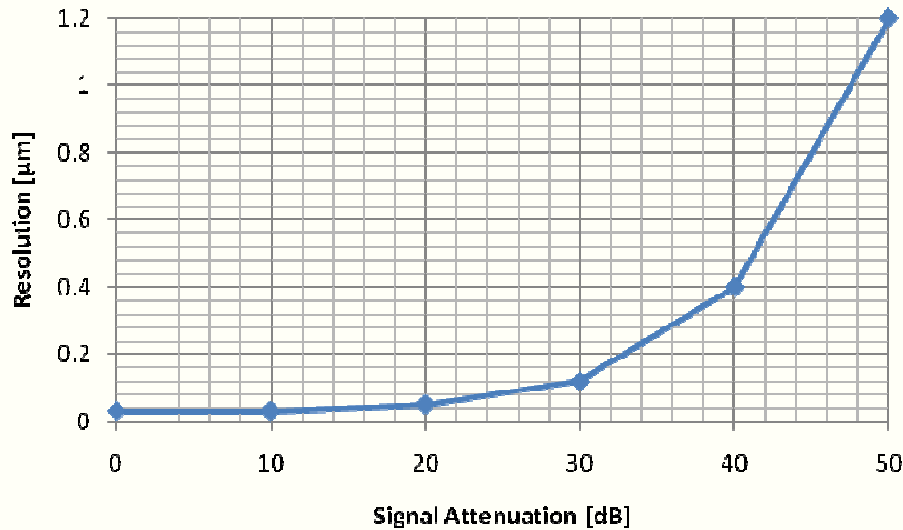


- Mini VME crate accommodating:
 - *Motorola* 5500 CPU
 - PMC CAN bus interface *ECAN-2*
 - Timing module TGF
 - *Echotek* digital receiver module



- BPM #54 prototype installation (temporary):
 - CAN bus remote control & CAL signal PLL unit (Fermilab)
 - **4 ch. Downconverter unit (SLAC)**

	Multi-turn	Orbit	Flash
Wide-Band	Samples: 4096 Samples/turn: 4 Turns: 1024 POSITION Intensity	Average Samples: 4096 Turns: 1024 POSITION (RMS & StdDev) Intensity (RMS & StdDev)	N th Sample (1) POSITION Intensity
Narrow-Band	Samples: 1280 μ sec/Sample: 158.73 Turns: 439600 POSITION Intensity	Average Samples: 126 (50 Hz Boxcar) Turns: 43273 POSITION (RMS & StdDev) Intensity (RMS & StdDev)	N th Sample (1) POSITION Intensity



Theoretical:

- ADC SNR: 75 dB
- Process gain: 40.4 dB
- NF 1st gain stage: ~ 1 dB
- CAL tone level: -10 dBm
- Splitter attenuation: 6 dB
- Effective gain: ~ 100 dB
- BPM sensitivity: 240 $\mu\text{m}/\text{dB}$
- Calculated equivalent resolution: ~ 20 nm

CAL tone resolution measurement on BPM #56: ~30 nm(!) equiv. resolution (no beam operation at ATF!, magnets off)