

# STATUS OF CLIC ACTIVITY AT IAP

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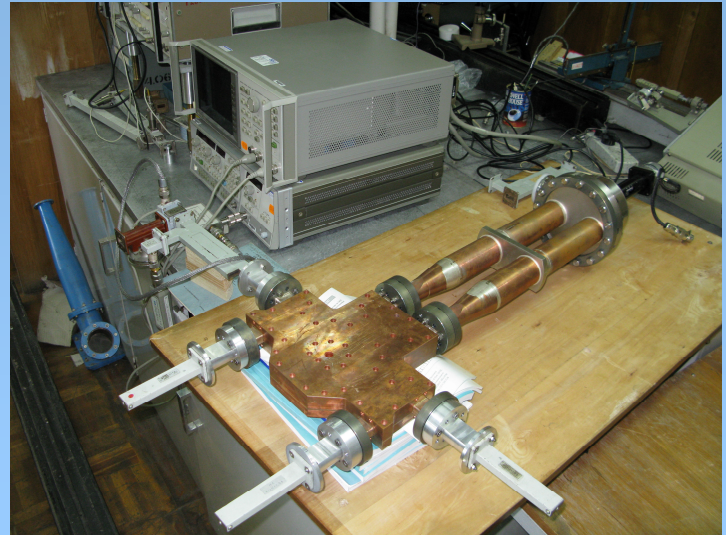
## Outline

1. Scope of activities
2. 12 GHz BMC
3. IAP – JINR pulse heating experiments at 30 GHz
4. 30 GHz multi-megawatt gyrotron and gyroklystron
5. Studies of multipactor discharges
  1. Methods to suppress multipactor on dielectric surface (windows and dielectric based accelerating structures)
  1. Multipactor on metallic surface (RF switches)
6. Future plans and prospects

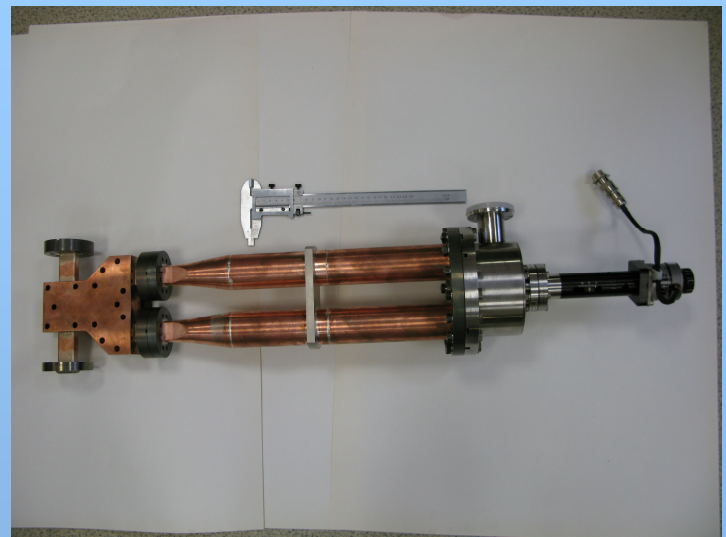
**Contracts with Gycom Ltd.:**

1. 30 GHz transmission line and RF components
2. 30 GHz SLED II PC
3. Length compensators for transmission lines
4. Pumping ports at big waveguide diameter
5. Vacuum valve
6. Attenuators and phase shifters at 30 GHz and 12 GHz
7. 12 GHz BMC

**Total: 10 contracts for last 3 years**

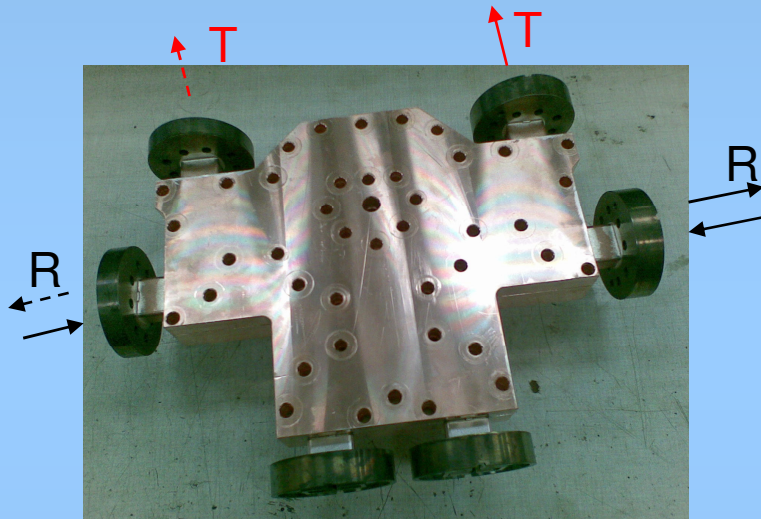


12 GHz attenuator

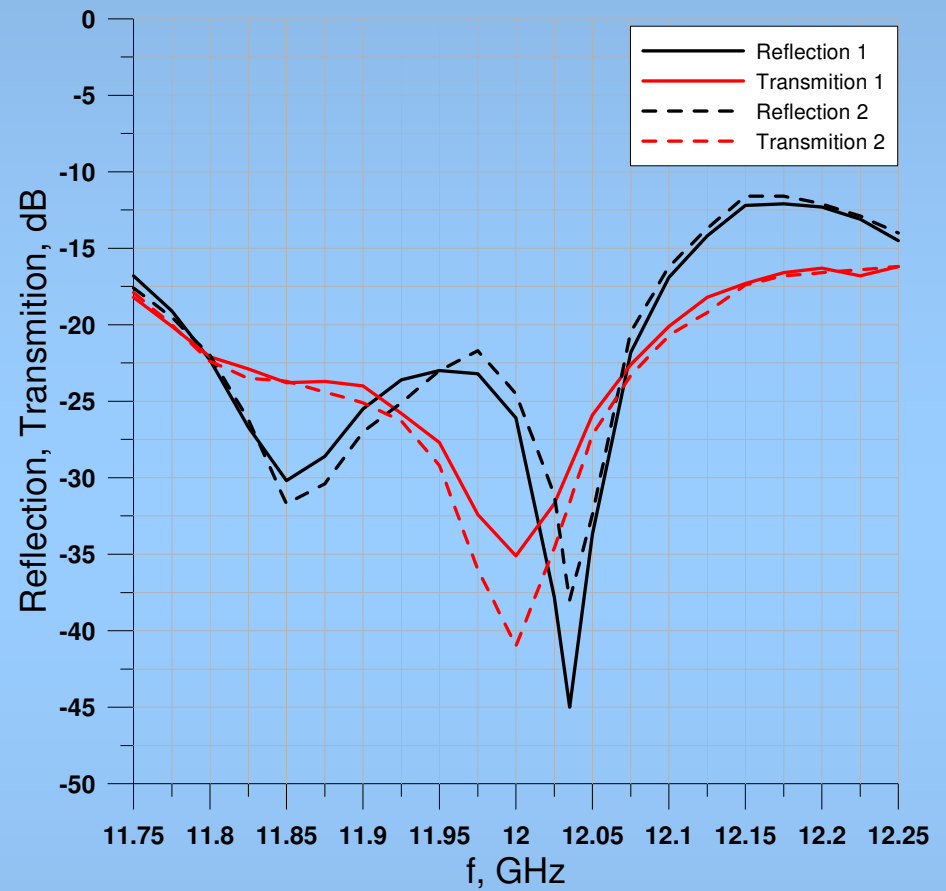


12 GHz phase shifter

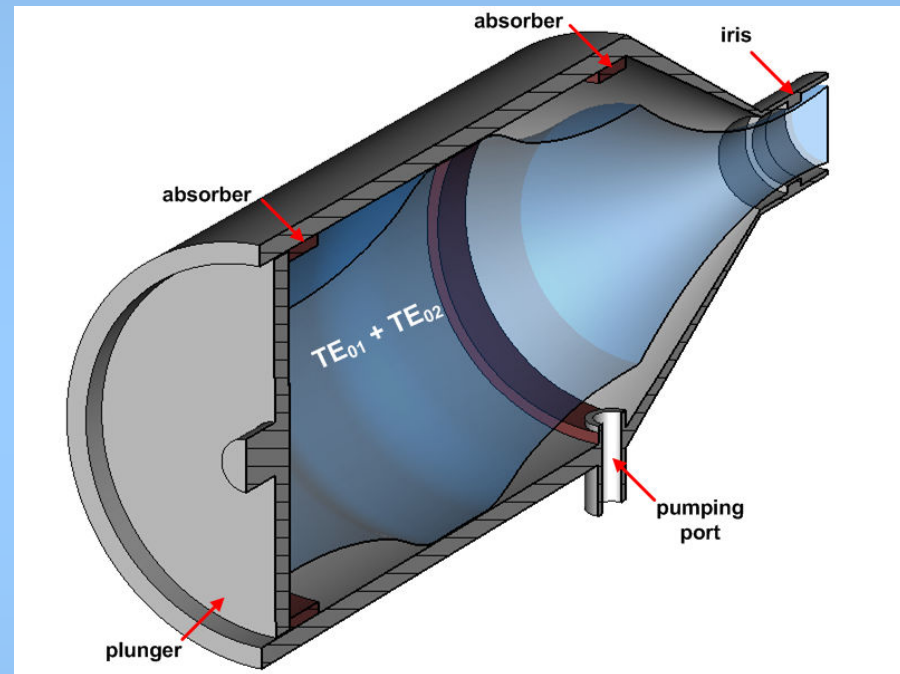
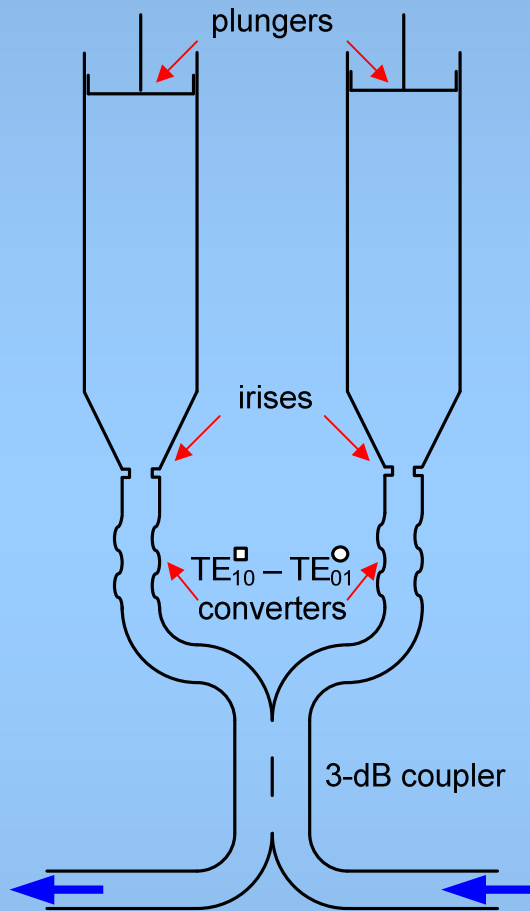
## The last contract component



12 GHz attenuator body

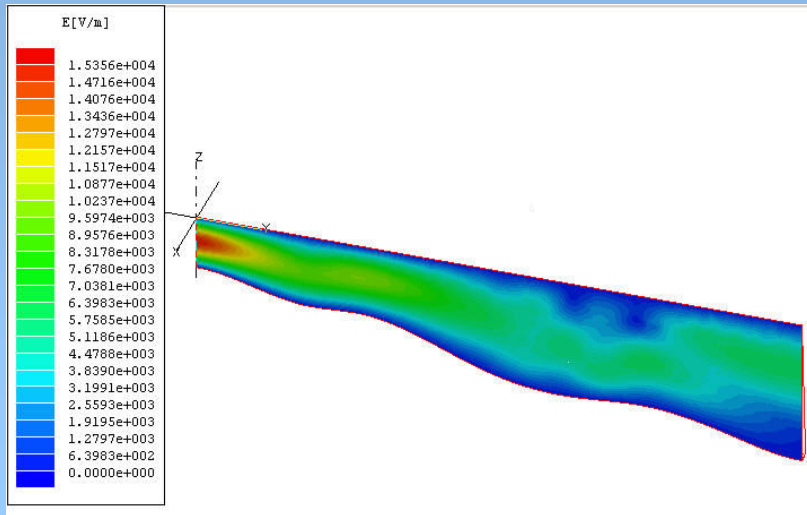


## 12 GHz BMC (under construction)

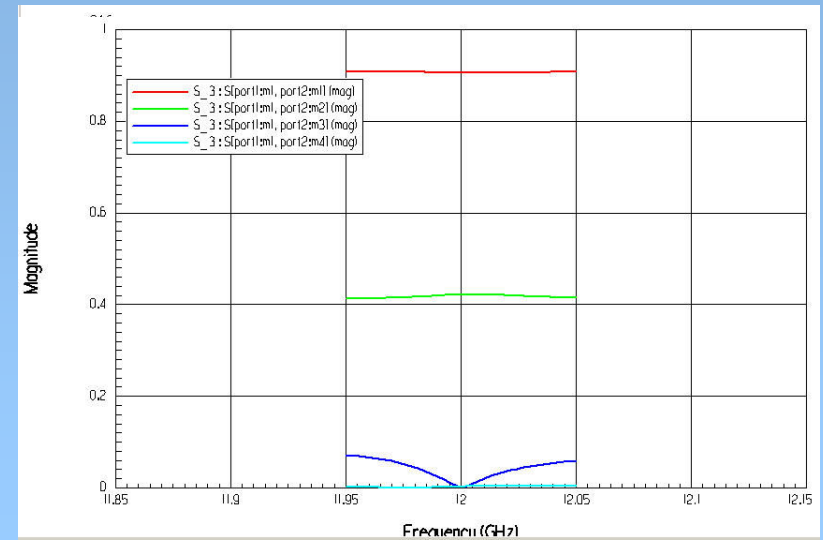


Scheme of BMC (beet mode pulse compressor).

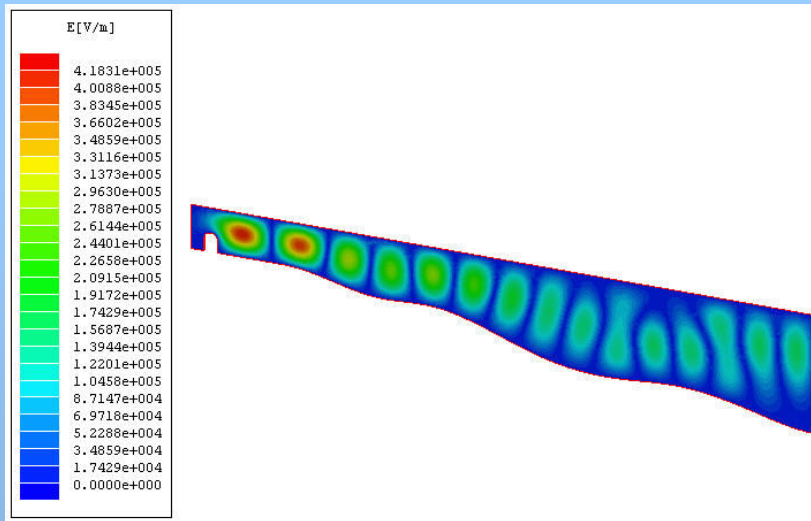




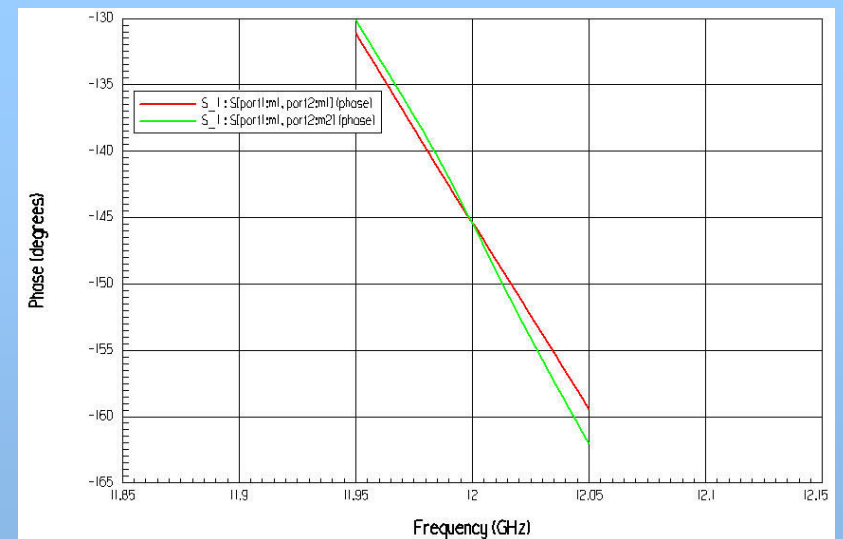
$TE_{01} - TE_{01} + TE_{02}$  beeting mode converter



Reflected and transmitted modes



Simulation of the BMC with coupling iris

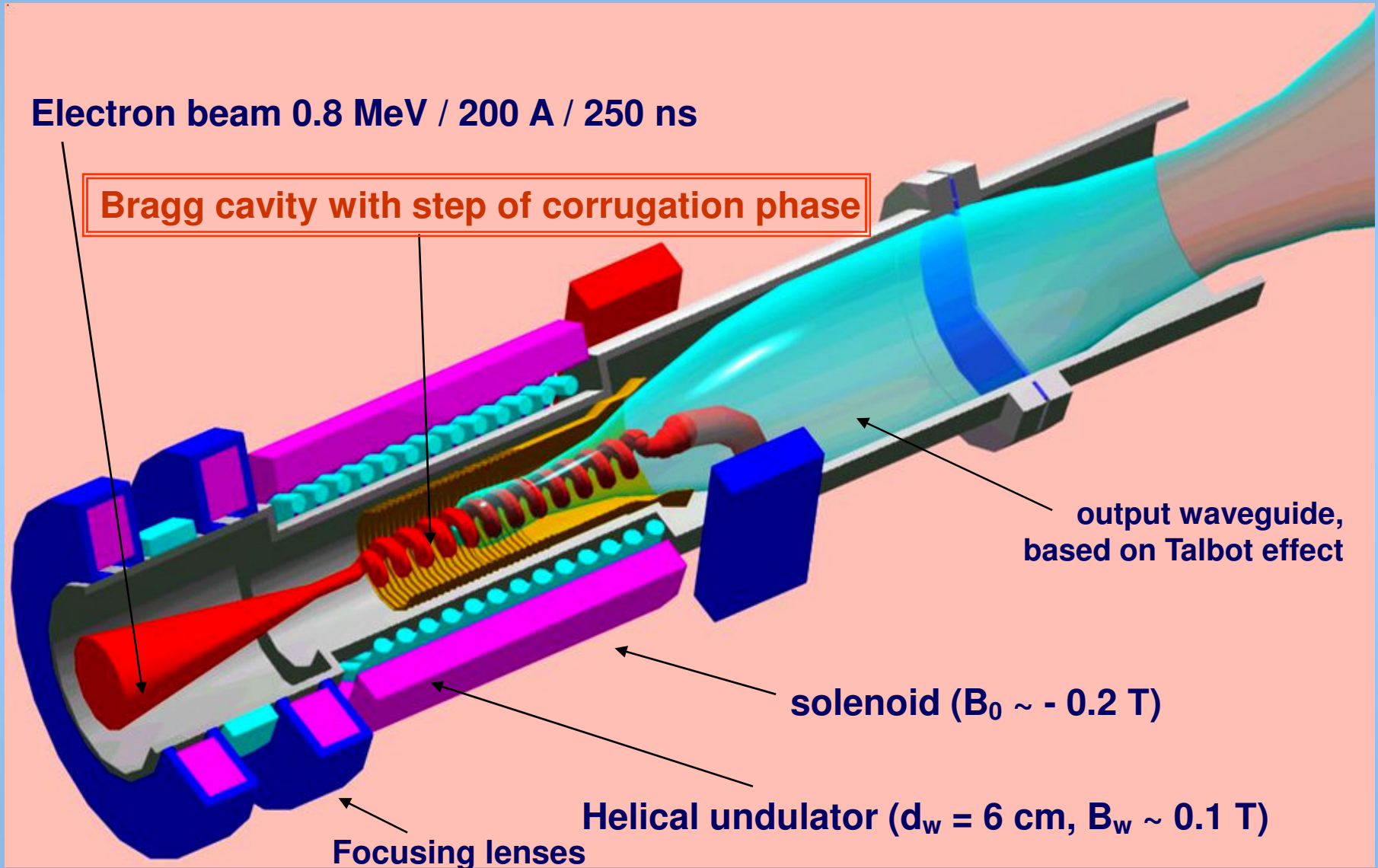


$TE_{01}$  and  $TE_{02}$  phases



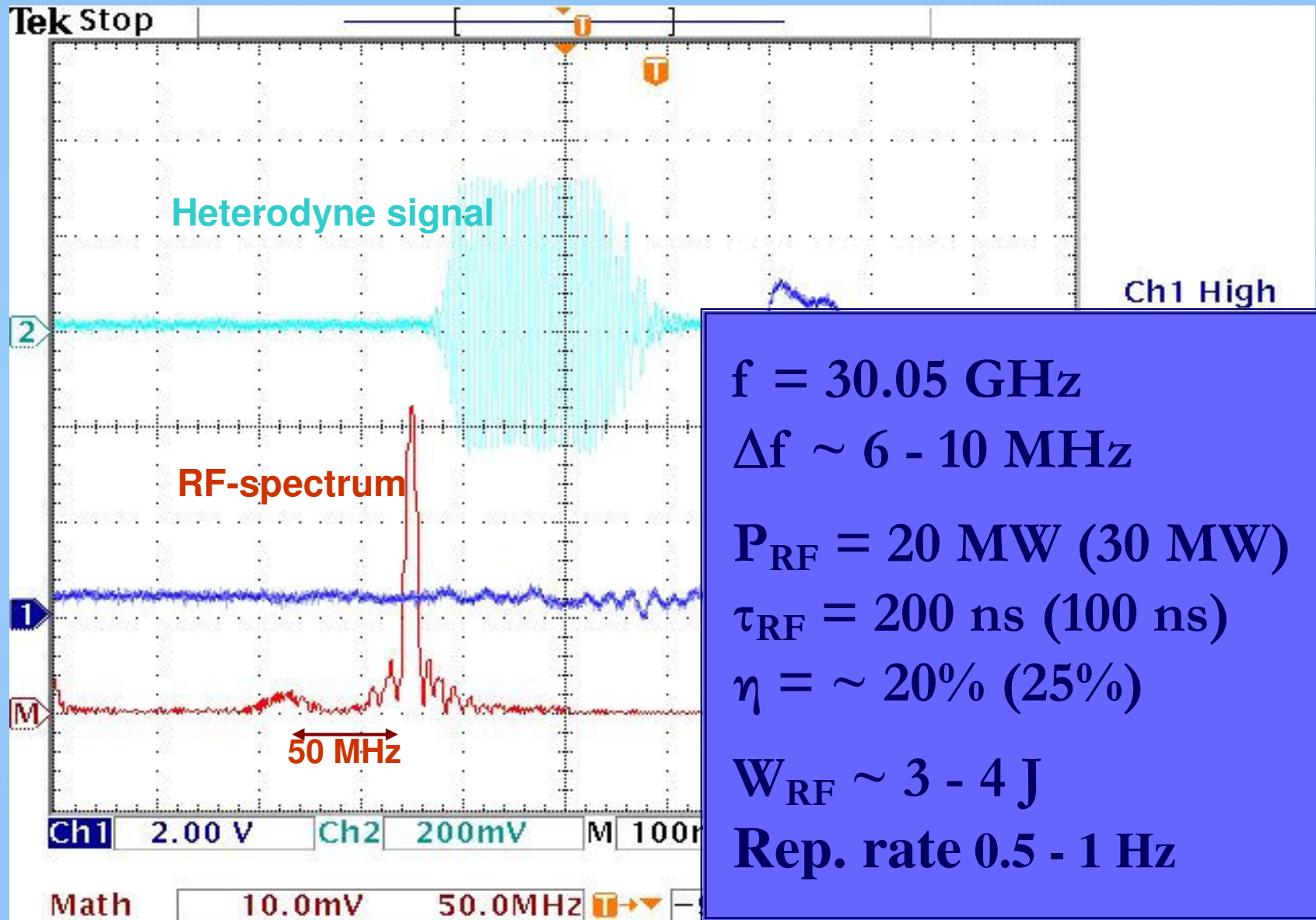
All necessary parts have been produced. We wait for the second stepping motor. Low power tests are scheduled on October - November 2009.

## Pulse heating experiments



Scheme of the 30 GHz FEM based on accelerator LIU-3000

# Experimental results



$$f = 30.05 \text{ GHz}$$

$$\Delta f \sim 6 - 10 \text{ MHz}$$

$$P_{\text{RF}} = 20 \text{ MW (30 MW)}$$

$$\tau_{\text{RF}} = 200 \text{ ns (100 ns)}$$

$$\eta = \sim 20\% (25\%)$$

$$W_{\text{RF}} \sim 3 - 4 \text{ J}$$

$$\text{Rep. rate } 0.5 - 1 \text{ Hz}$$



# Experimental investigations of copper degradation effects caused by RF pulsed heating by means of 30 GHz FEM

Output section of FEM

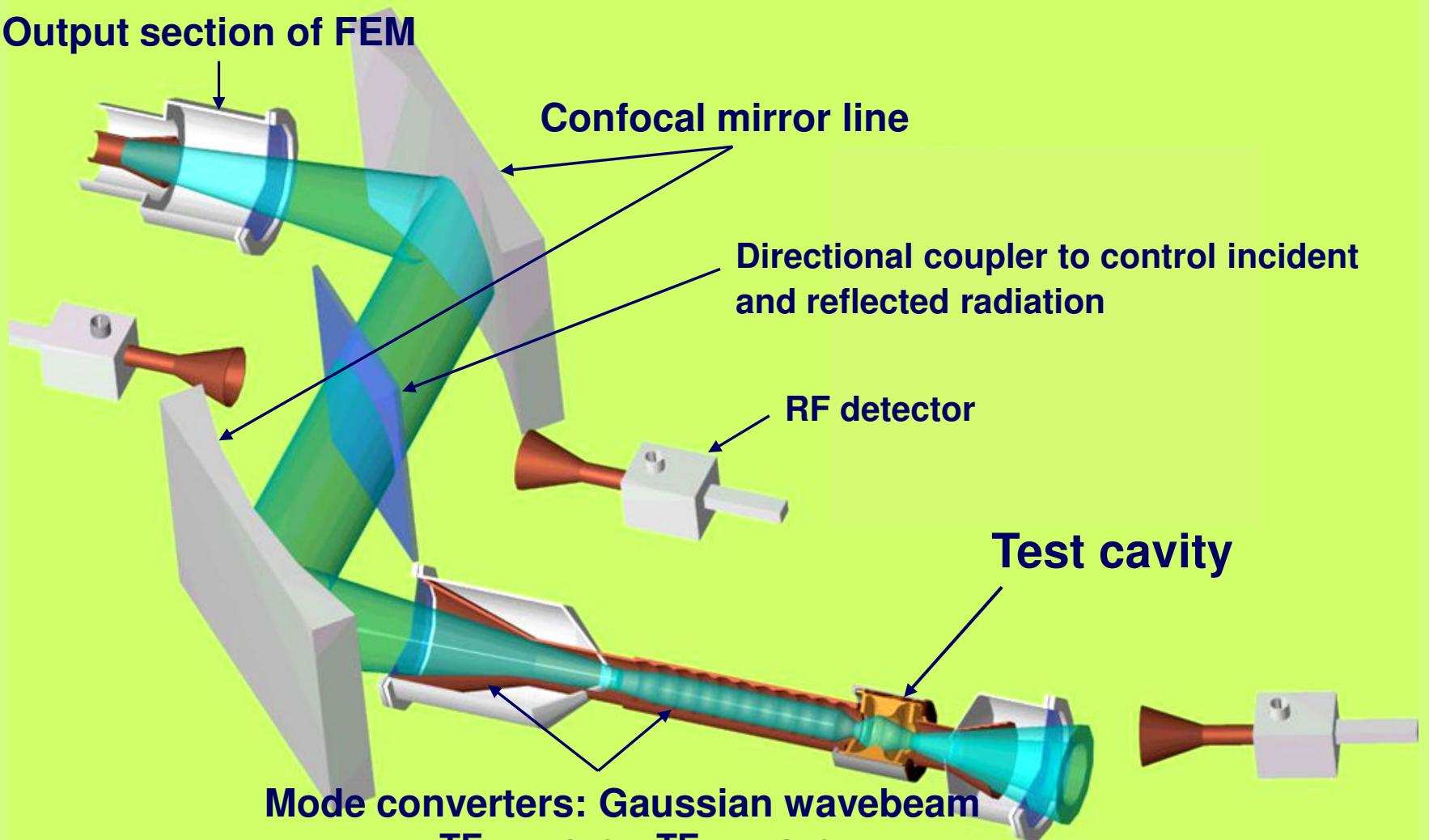
Confocal mirror line

Directional coupler to control incident and reflected radiation

RF detector

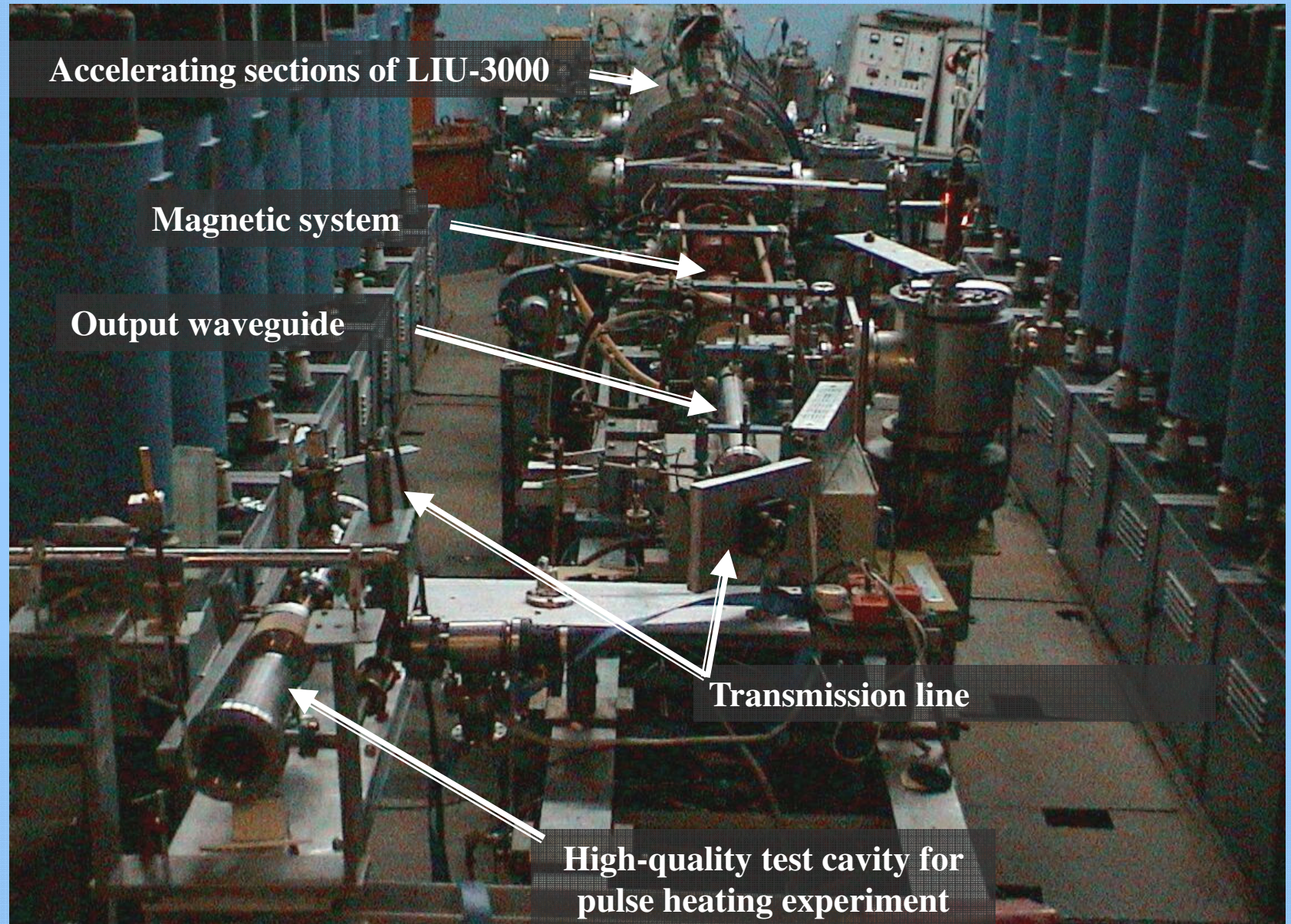
Test cavity

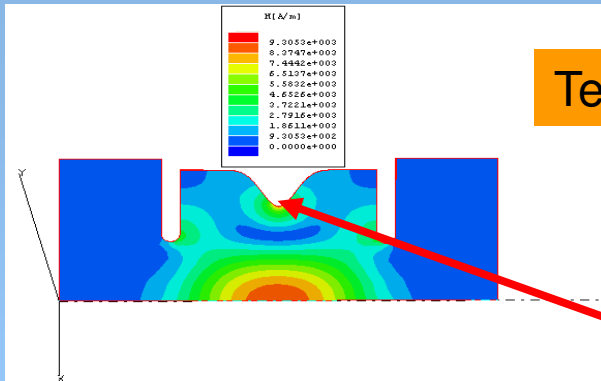
Mode converters: Gaussian wavebeam  
–  $TE_{1,1}$  wave –  $TE_{0,1}$  wave





## FEM on a base of LIU-3000

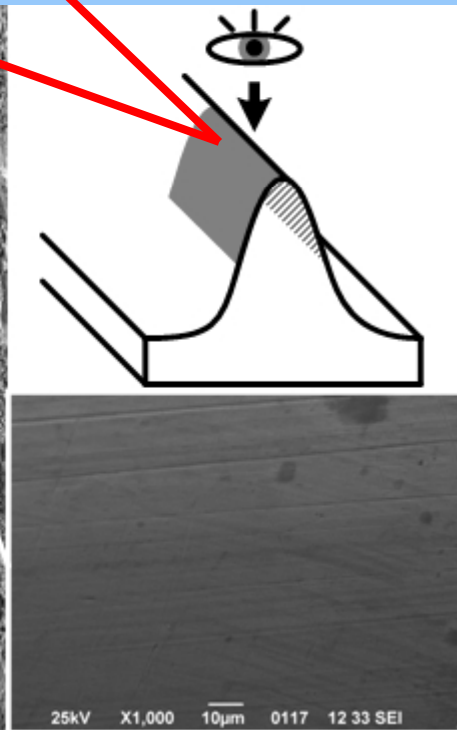
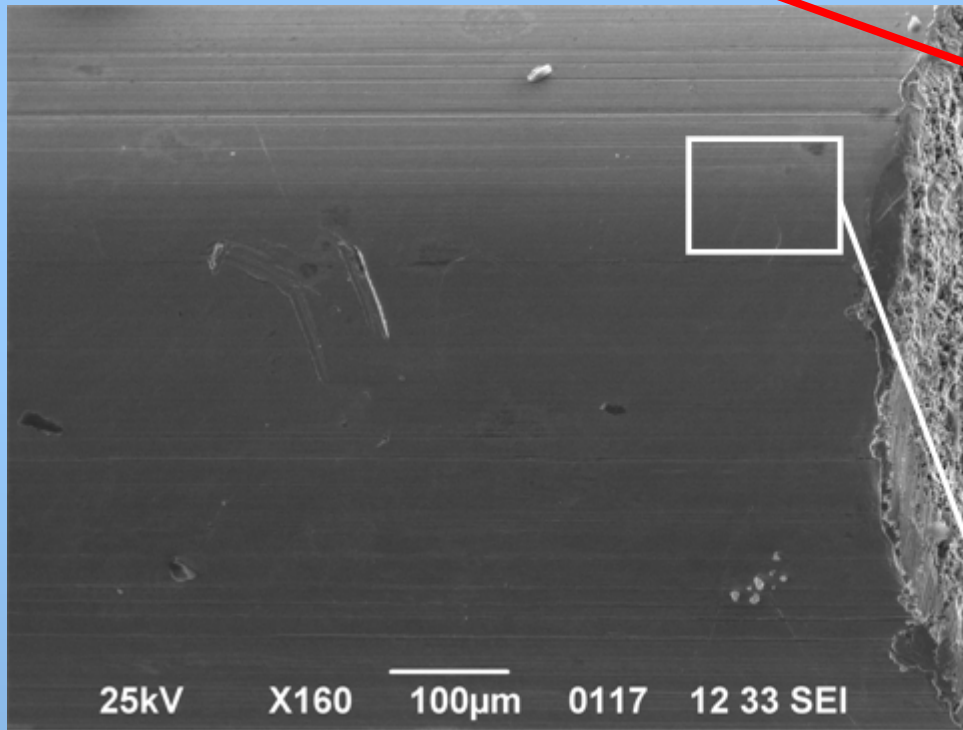




Test cavity

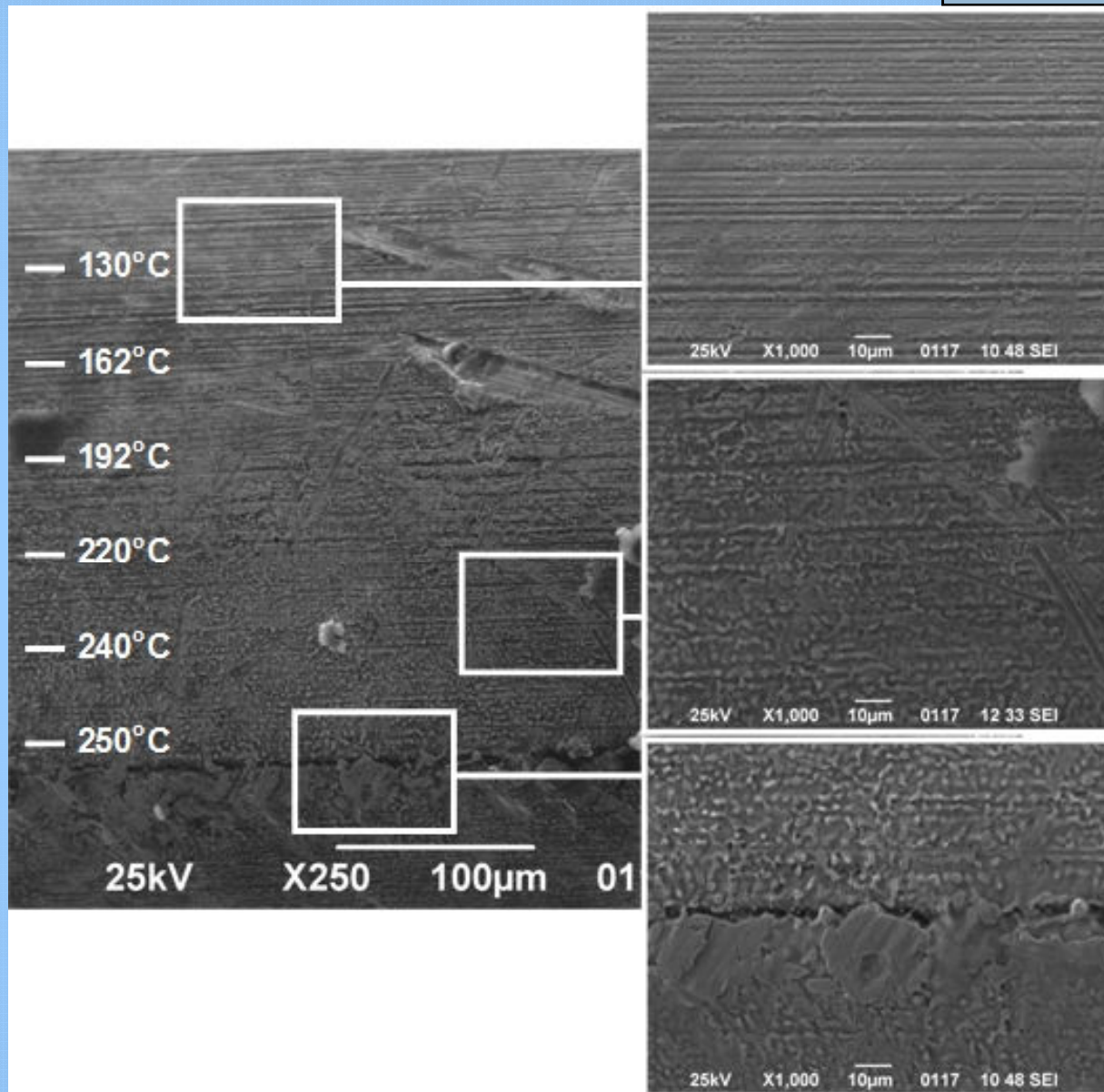


Magnetic field

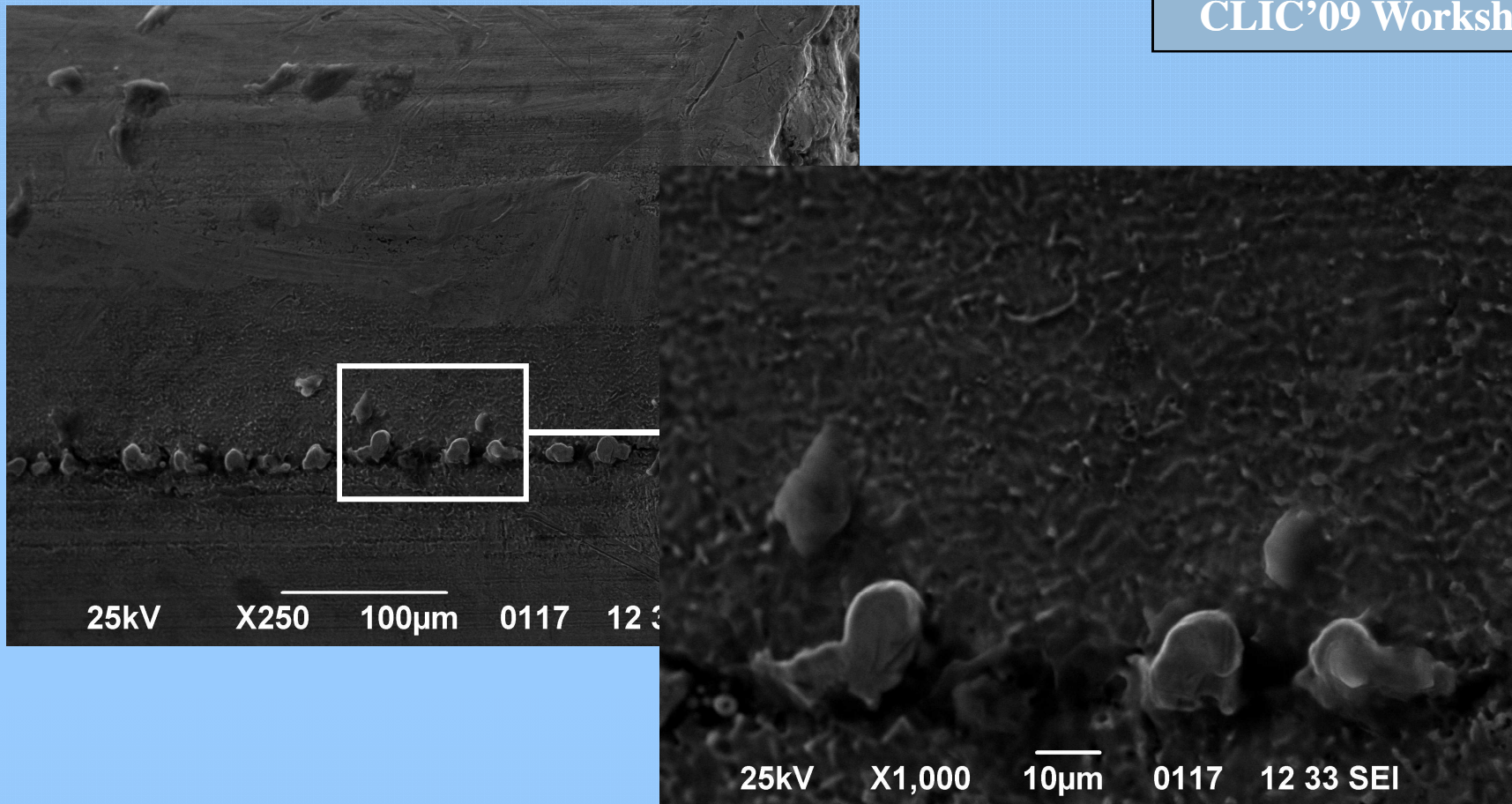


Photograph of the unexposed surface





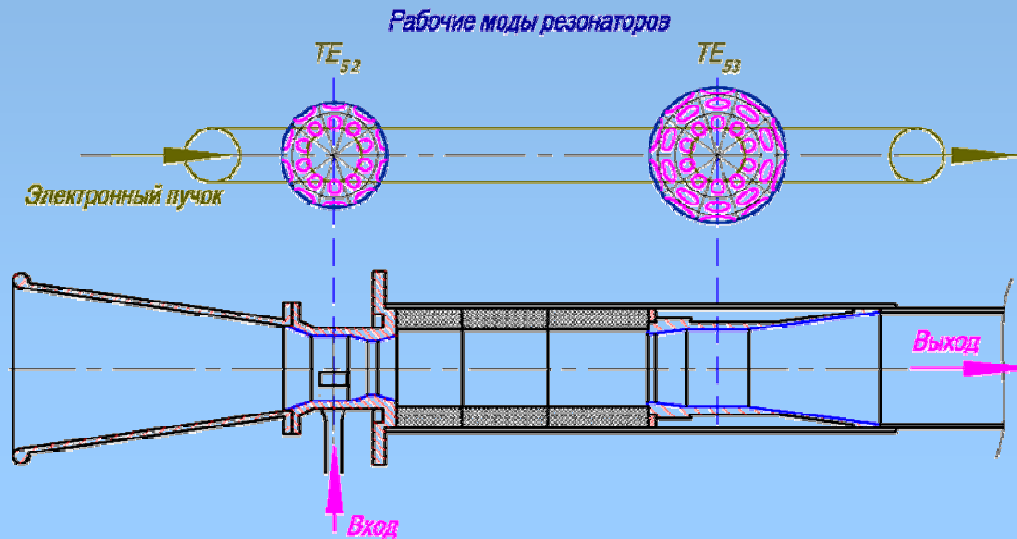
Photographs of the exposed surface (250° C,  $6 \times 10^4$  RF pulses)



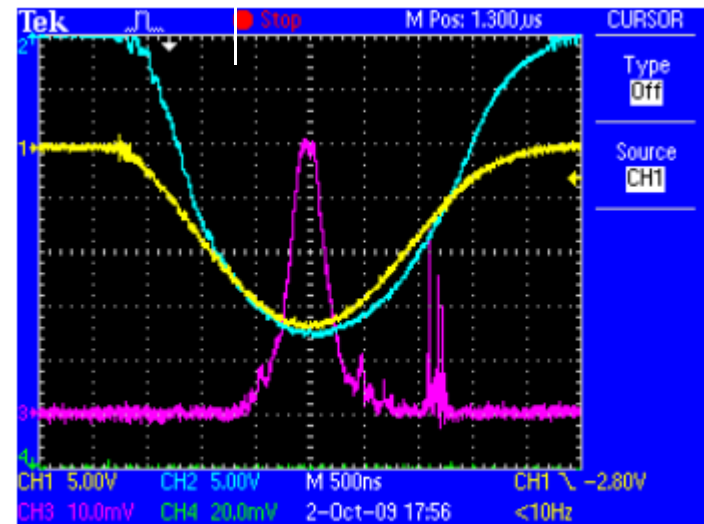
Breakdown marks

The carried out experiments on pulse heating at 30 GHz show that temperature rise  $\sim 50^\circ\text{C}$  per pulse does not spoil cavity surface ( $N < 10^5$ ). Temperature rise  $200\text{-}250^\circ\text{C}$  leads to dramatic degradation of the tested copper surface and causes very frequent breakdown ( $\text{BDR} = 0.3\text{-}0.5$ ) if total number of RF pulses reaches  $6 \cdot 10^4$ .

## 30 GHz gyrotron/gyroklystron



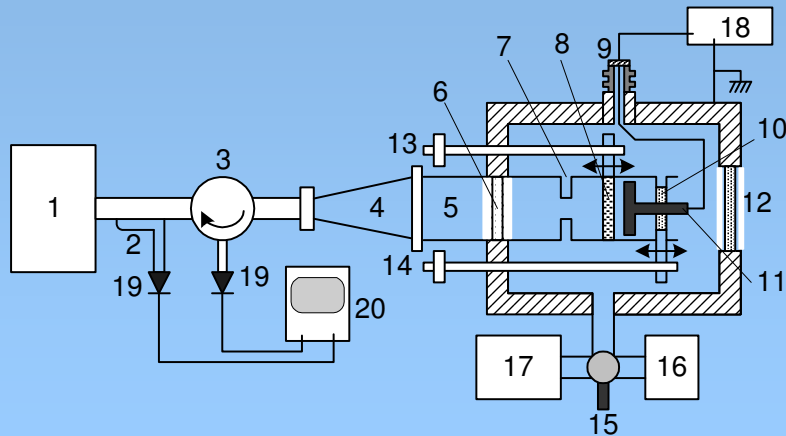
**$U=300-450$  кV,**  
 **$I=180$  A,**  
 **$\tau=0.5-1.5$   $\mu$ s,**  
 **$f_{\text{rep}}=1-10$  Hz,**  
 **$F=30$  GHz**  
**RF power = 10-15 MW.**



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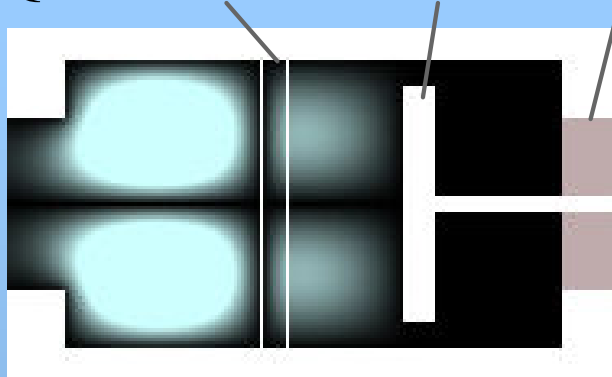
## IAP experiments with multipactor discharge in X – band



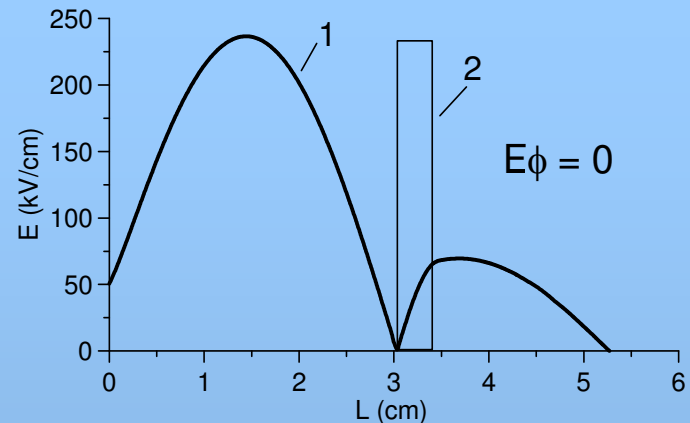
Experimental setup

1 - magnetron, 2 - directional coupler, 3 - circulator, 4 - mode converter, 5 - circular waveguide, 6 - microwave window, 7 - diaphragm, 8 - studied dielectric disk, 9 - high voltage input, 10 - insulator, 11 - electrode (back wall of the resonator), 12 - observation window, 13 and 14 - disk and electrode transfer mechanisms, respectively, 15 - pressure gauge, 16 - mechanical pump, 17 - ion pump, 18 - high-voltage source, 19 - microwave detector, 20 - oscilloscope

Quartz disk    Electrode    Isolator

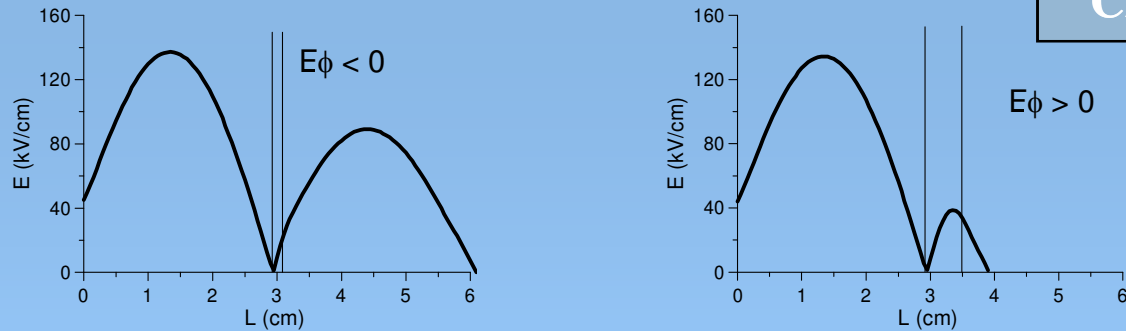


$TE_{012}$

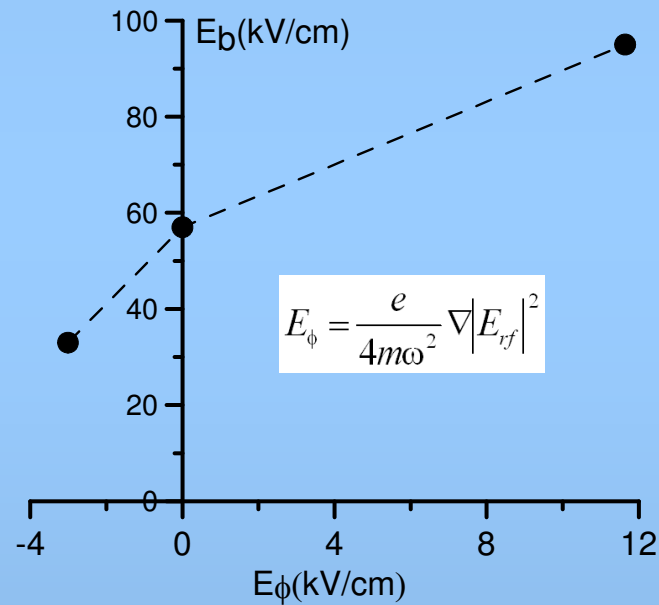


1 – amplitude of the RF field for an incident power 100 kW  
2 – quartz disk

Distribution of the microwave electric field in the resonator



Distribution of the microwave electric field

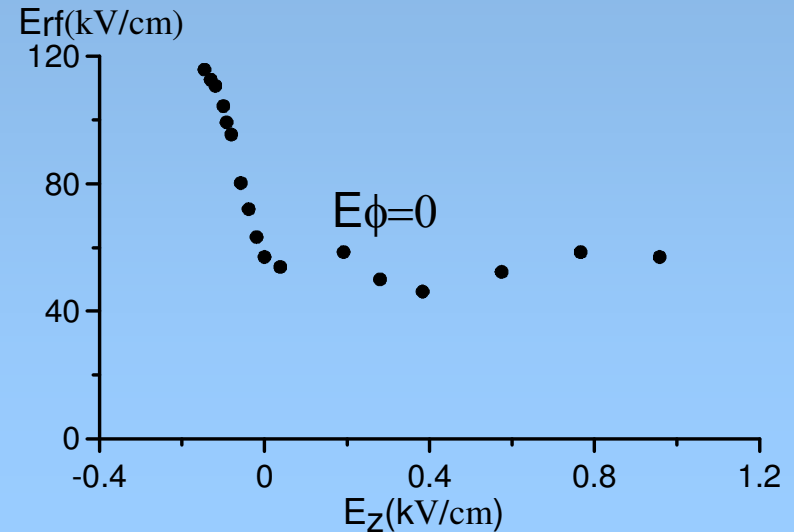
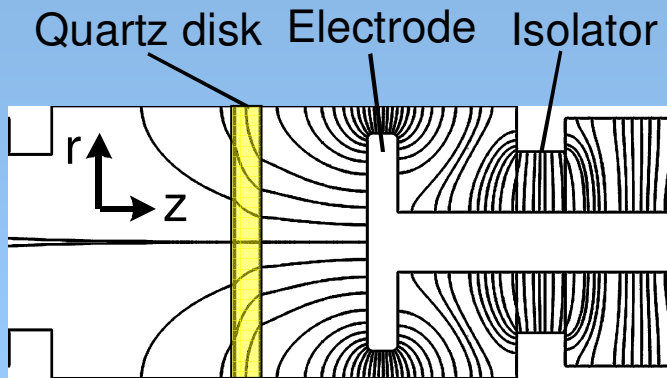


Dependence threshold value of ponderomotive force

[1] - M.A. Lobaev, O.A. Ivanov, V.A. Isaev, A.L. Vikharev, Tech. Phys. Lett. v. 35, N 12.

[2] - O.A. Ivanov, M.A. Lobaev, V.A. Isaev, A.L. Vikharev, Physical Revue ST AB (in press)

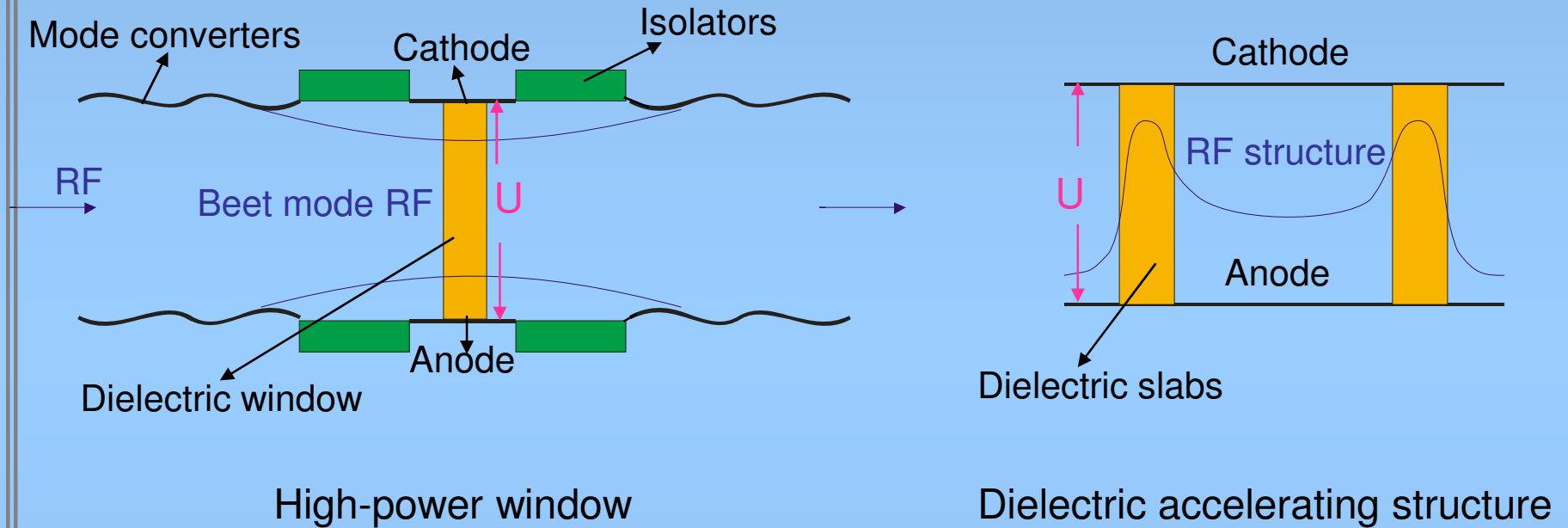
## Influence of external DC bias



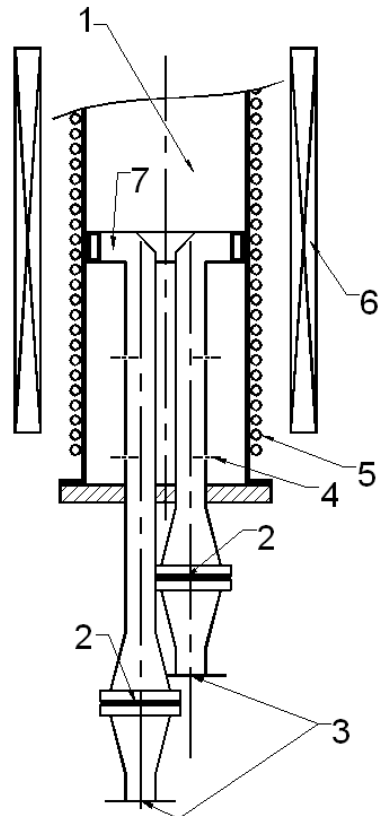
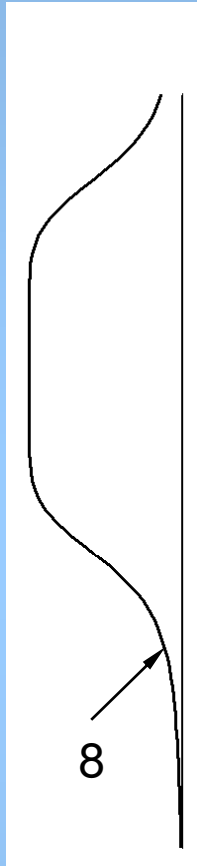
Dependence of the multipactor threshold on the amplitude of the electrostatic field

1. The experiments performed showed that one can effectively suppress the multipactor discharge on a dielectric.
2. The effects make it possible to use such an undesirable phenomenon as a multipactor for practical purposes, e.g., in high-power microwave switches intended to modulate the Q-factor in active compressors of microwave pulses.

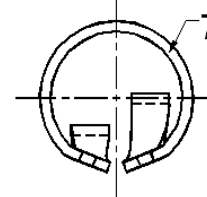
## Raise of multipactor threshold by means of external DC bias



# Multipactor at metallic surface with external static magnetic field

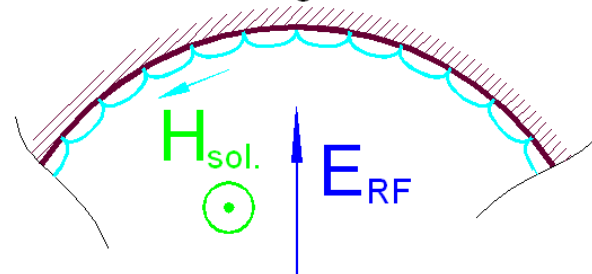


Waveguide of rectangular  
cross section 23x5  
(upper view)



$\lambda = 3.3$  cm,  
diameter of the  
waveguide ring is near  
100 mm

Electron trajectories  
at the waveguide surface



10 GHz 200 kW magnetron

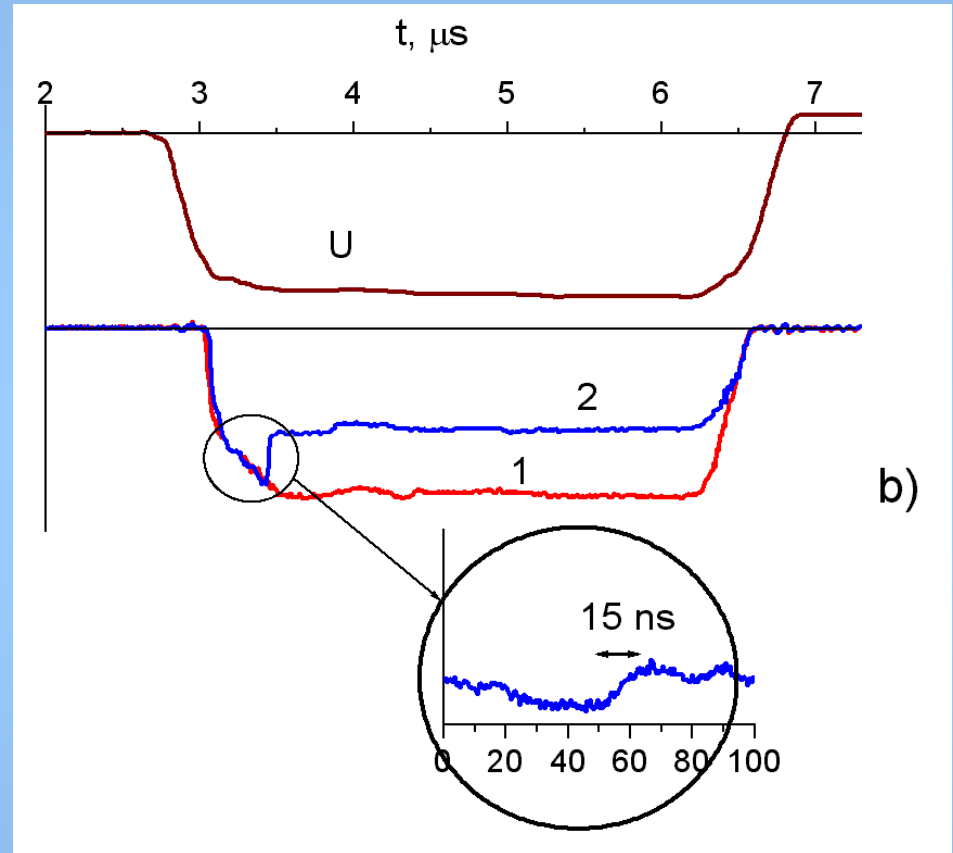
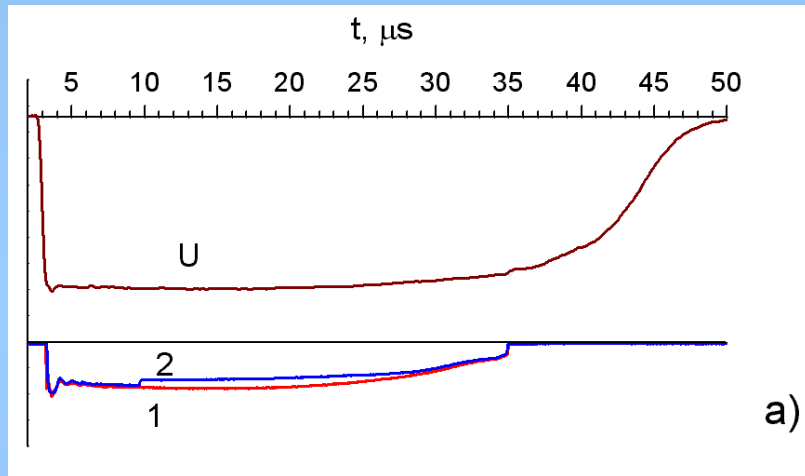
1 – vacuum casing; 2 - RF window; 3 – input and output waveguide flange; 4 – openings for waveguide evacuation; 5 – heater; 6 – pulse solenoid; 7 – waveguide bended into a ring; 8 – magnetic field profile





**Tested waveguide**

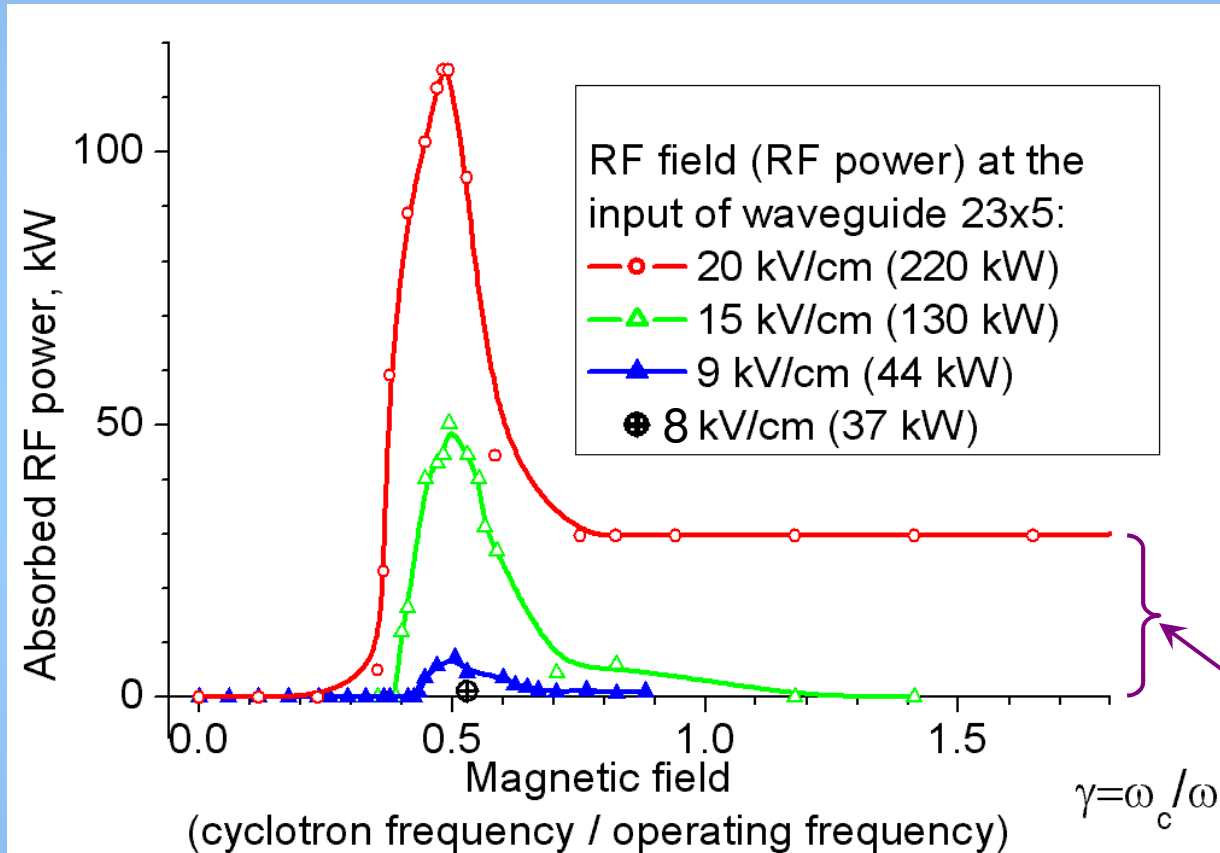
# Transmitted RF power at the absence and presence of multipactor discharge



Traces of output power at the absence (1) and the presence (2) of multipactor discharge. The input power is 44 kW (a) and 220 kW (b)

U – voltage pulse

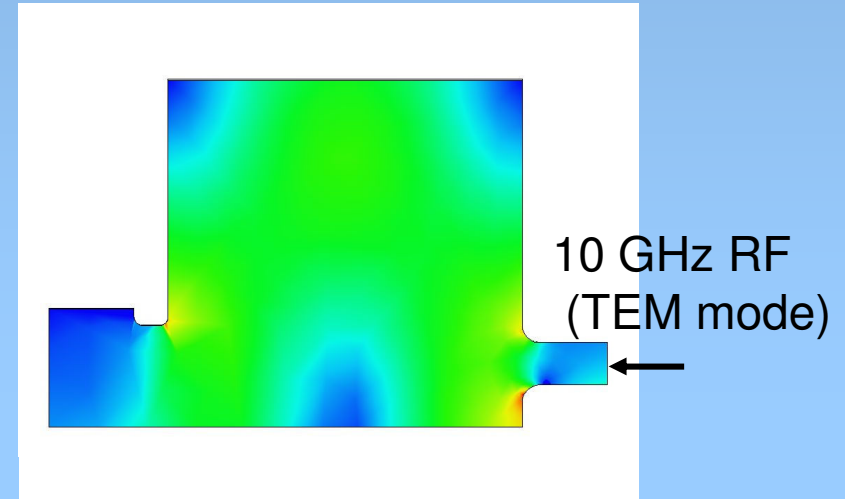
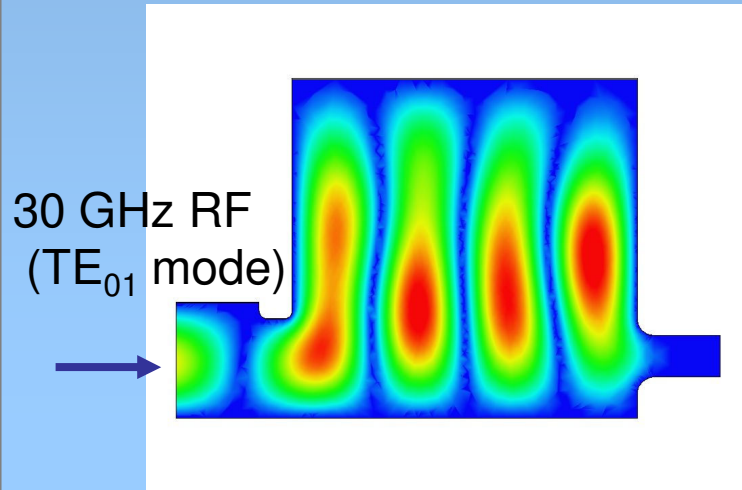
# Dependence of the absorbed RF power on the static magnetic field



Multipactor absorption in the input and output waveguides near the brink of solenoid

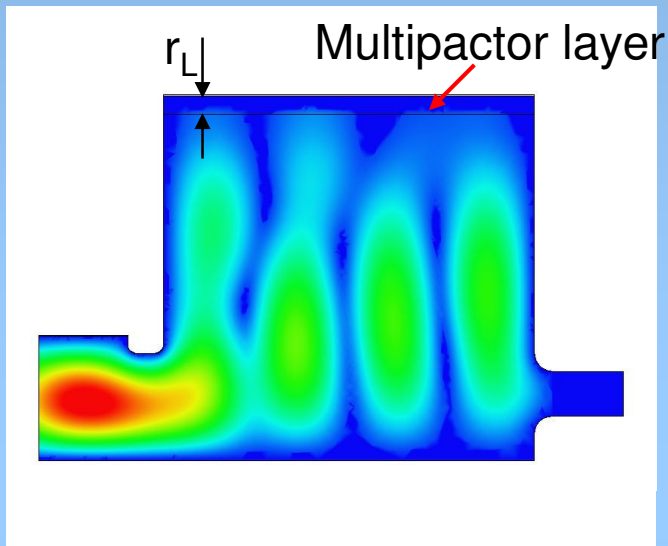
Magnetic field can be used for slow ( $\sim 1 \mu\text{s}$ ) RF switching

## Fast active RF switch (phase shifter) based on induced multipactor



High-Q 30 GHz cavity (operating RF)    The same cavity at 10 GHz, low-Q (switching RF)

10 GHz radiation of kW power level initiates multipactor,  
30 GHz operating radiation of multi-megawatt power level is scattered and absorbed by the prepared multipactor.  
Switching time is 10-20 ns.

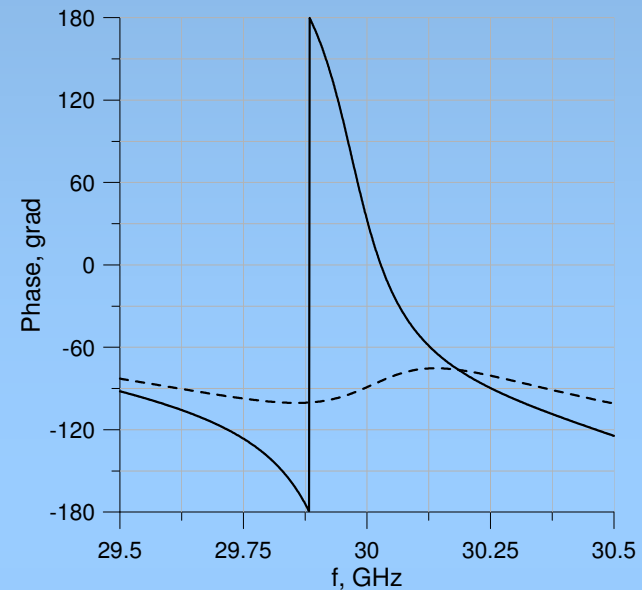


Simulation of multipactor influence

$$\varepsilon = 1 - \frac{\omega_{pe}^2}{(\omega + i\omega_c)^2},$$

$$\omega_{pe} = \left( \frac{4\pi \cdot N_e e^2}{m} \right)^{1/2}, \quad \omega_c = \frac{eH}{mc}.$$

$r_L$  – is Larmor radius.



Phase switching by multipactor

Solid curve is the phase before multipactor,  
Dashed curve is the phase under multipactor.



## Conclusion

We will do the best in order to complete all day-to-day contracts, to solve all technical problems, and hope to continue collaboration with CLIC.